

Linear Quantum Systems

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Outline

- [Background and Motivation
- [Linear Quantum Models
- [Dissipation Properties
- [H-Infinity Controller Synthesis
- [Robust Stability
- [Examples

Background and Motivation

- [The need for robustness in quantum control systems
- [The “H-infinity” approach to robust control system design

Linear Quantum Models

We consider noncommutative stochastic systems of the form

$$\begin{aligned}dx(t) &= Ax(t)dt + Bdw(t) \\ dz(t) &= Cx(t)dt + Ddw(t)\end{aligned}$$

where A , B , C and D are real matrices, and

$$x(t) = \begin{bmatrix} x_1(t) \\ \vdots \\ x_n(t) \end{bmatrix}$$

is a vector of possibly noncommutative plant variables.

The initial system variables $x(0)$ are Gaussian with state ρ , and satisfy the commutation relations

$$[x_j(0), x_k(0)] = C_{jk}^{xx} = 2i\Theta_{jk}, \quad j, k = 1, \dots, n,$$

where Σ is a real antisymmetric matrix.

For example, a system with one classical variable and two conjugate quantum variables is characterized by

$$\Theta = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & -1 & 0 \end{bmatrix}.$$

The vector quantity w describes input channels and is assumed to admit the decomposition

$$dw(t) = \beta_w(t)dt + d\tilde{w}(t)$$

where $\beta_w(t)$ is the self-adjoint finite variation part, and $\tilde{w}(t)$ is the (Gaussian) noise part of $w(t)$ with Ito table

$$d\tilde{w}(t)d\tilde{w}^T(t) = F_{\tilde{w}}dt,$$

where $F_{\tilde{w}}$ is a non-negative Hermitian matrix.

For instance,

$$F_{\tilde{w}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & i \\ 0 & -i & 1 \end{bmatrix}$$

describes a noise vector with one classical component and a pair of conjugate quantum Gaussian noises.

Physical systems

Preservation of commutation relations imposes constraints on plant matrices A, B, C, D :

Assume $[x_i(t), \beta_{w,j}(t)] = C_{ij}^{x\beta_w}$ for all $t \geq 0$. Then

$$[x_i(0), x_j(0)] = C_{ij}^{xx} \text{ implies } [x_i(t), x_j(t)] = C_{ij}^{xx}$$

for all $t \geq 0$ if and only if

$$AC^{xx} + C^{xx}A^T - B(C^{x\beta_w})^T + C^{x\beta_w}B^T + 2BT_{\tilde{w}}B^T = 0.$$

Physical realizability

When seeking to build controllers from linear models we need to know when such a model is physically realizable.

We regard all classical systems as physically realizable, at least approximately via classical electronics.

We shall say that a system is *physically realizable* if it corresponds to a completely positive evolution.

The commutation relations can be used to characterize physical realizability, for example:

Assume that Σ is invertible and n is even, and $C^{x\beta_w} = 0$. Then the system is physically realizable if and only if the condition

$$AC^{xx} + C^{xx}A^T + 2BT_{\tilde{w}}B^T = 0$$

holds.

Dissipation Properties

- [We wish to characterize the effect of inputs on system behavior
e.g. effect of disturbances on performance
- [We generalize the notions of “dissipation” widely used in classical control and formalized by J.C. Willems, 1972.
- [This keeps track of power flows and stored energy

Definition

Given an operator valued quadratic form

$$r(x, \beta_w) = [x^T \beta_w^T] R \begin{bmatrix} x \\ \beta_w \end{bmatrix}$$

where

$$R = \begin{bmatrix} R_{11} & R_{12} \\ R_{12}^T & R_{22} \end{bmatrix}$$

is a given real symmetric matrix.

We say the system is *dissipative with supply rate* $r(x, \beta_w)$ if there exists a positive operator valued quadratic form $V(x) = x^T X x$ (where X is a real positive definite symmetric matrix) and a constant $\lambda > 0$ such that

$$\langle V(x(t)) \rangle + \int_0^t \langle r(x(s), \beta_w(s)) \rangle ds \leq \langle V(x(0)) \rangle + \lambda t \quad \forall t > 0,$$

for all Gaussian ρ .

We say that the system is *strictly dissipative* if there exists a constant $\epsilon > 0$ such that the above inequality holds with the matrix R replaced by the matrix $R + \epsilon I$.

Theorem

The system is dissipative with supply rate $r(x, \beta_w)$ if and only if there exists a real positive definite symmetric matrix X such that the following matrix inequality is satisfied:

$$\begin{pmatrix} A^T X + XA + R_{11} & R_{12} + XB \\ B^T X + R_{12}^T & R_{22} \end{pmatrix} \leq 0.$$

Furthermore, the system is strictly dissipative if and only if there exists a real positive definite symmetric matrix X such that the following matrix inequality is satisfied:

$$\begin{pmatrix} A^T X + XA + R_{11} & R_{12} + XB \\ B^T X + R_{12}^T & R_{22} \end{pmatrix} < 0$$

Moreover, if either of the above holds then the required constant $\lambda \geq 0$ can be chosen as

$$\lambda = \text{tr} \left[\begin{bmatrix} B^T \\ G^T \end{bmatrix} X \begin{bmatrix} B & G \end{bmatrix} F \right]$$

where the matrix F is defined by the following relation:

$$F dt = \begin{bmatrix} dw \\ dv \end{bmatrix} \begin{bmatrix} dw^T & dv^T \end{bmatrix}.$$

The proof depends on the following identity

$$\langle V(x(t)) \rangle \triangleq (\rho \otimes \phi)(V(x(t))) = \langle \rho, E_0[V(x(t))] \rangle,$$

where E_0 denotes expectation with respect to ϕ , and on the following

Lemma

Consider a real symmetric matrix X and corresponding operator valued quadratic form $\eta^T X \eta$. Then the following statements are equivalent:

1. There exists a constant $\lambda \geq 0$ such that

$$\langle \rho, \eta^T X \eta \rangle \leq \lambda$$

for all Gaussian states ρ .

2. The matrix X is negative semidefinite.

For H^∞ control, we need the following special case:

Definition

The system is said to be *Bounded Real* if it is dissipative with supply rate

$$\begin{aligned} r(x, \beta_w) &= \beta_z^T \beta_z - \beta_w^T \beta_w \\ &= [x^T \beta_w^T] \begin{bmatrix} C^T C & C^T D \\ D^T C & D^T D - I \end{bmatrix} \begin{bmatrix} x \\ \beta_w \end{bmatrix}. \end{aligned}$$

It is *Strictly Bounded Real* if it is strictly dissipative with this supply rate.

Corollary

The system is bounded real if and only if there exists a positive definite symmetric matrix $X \in \mathbf{R}^{n \times n}$ such that the following matrix inequality is satisfied:

$$\begin{pmatrix} A^T X + XA + C^T C & C^T D + XB \\ B^T X + D^T C & D^T D - I \end{pmatrix} \leq 0.$$

Furthermore, the quantum stochastic system is strictly bounded real if and only if there exists a positive definite symmetric matrix $X \in \mathbf{R}^{n \times n}$ such that the following matrix inequality is satisfied:

$$\begin{pmatrix} A^T X + XA + C^T C & C^T D + XB \\ B^T X + D^T C & D^T D - I \end{pmatrix} < 0.$$

Moreover, in both cases the required constant $\lambda \geq 0$ can be chosen as

$$\lambda = \text{tr} \left[\begin{bmatrix} B^T \\ G^T \end{bmatrix} X \begin{bmatrix} B & G \end{bmatrix} F \right].$$

Corollary

The following statements are equivalent

- 1. The system is strictly bounded real.*
- 2. A is a stable matrix and $\|C(sI - A)^{-1}B + D\|_{\infty} < 1$.*
- 3. $I - D^T D > 0$ and there exists a positive definite matrix $X > 0$ such that*

$$\begin{aligned} &A^T X + XA + C^T C \\ &+ (XB + C^T D)(I - D^T D)^{-1}(B^T X + D^T C) < 0. \end{aligned}$$

- 4. The algebraic Riccati equation*

$$\begin{aligned} &A^T X + XA + C^T C \\ &+ (XB + C^T D)(I - D^T D)^{-1}(B^T X + D^T C) = 0 \end{aligned}$$

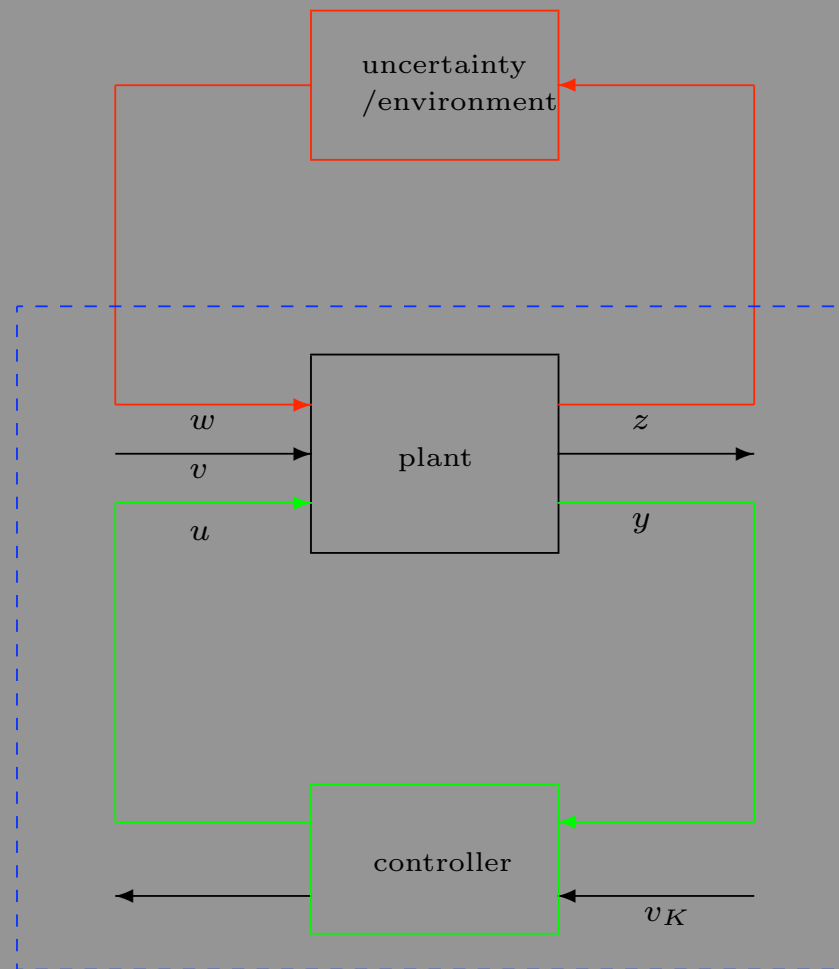
has a stabilizing solution $X \geq 0$.

Furthermore, if these statements hold then $0 < X$.

H-Infinity Controller Synthesis

Problem:

- [Given a plant and gain g , find a controller such that the closed loop system from w to z has gain less than g .



(to reduce effect of
environment/uncertainty)

Idea of solution:

- [Form a closed loop system consisting of the plant and controller (of prescribed form - a standard approach)
- [Apply the strict bounded real lemma
- [This (partly) determines linear equations for controller
- [Complete, if possible, physical realization of controller

Plant model

$$dx(t) = Ax(t)dt + B_0dv(t) + B_1dw(t) + B_2du(t);$$

$$x(0) = x;$$

$$dz(t) = C_1x(t)dt + D_{12}du(t);$$

$$dy(t) = C_2x(t)dt + D_{20}dv(t) + D_{21}dw(t)$$

Controller model

$$d\xi(t) = A_K \xi(t)dt + B_{K1}dv_K(t) + B_K dy(t)$$

$$du(t) = C_K \xi(t)dt + B_{K0}dv_K(t)$$

Closed loop system

Write

$$\eta(t) = \begin{bmatrix} x(t) \\ \xi(t) \end{bmatrix}.$$

Then

$$\begin{aligned} d\eta(t) &= \tilde{A}\eta(t)dt + \tilde{B}dw(t) + \tilde{G}d\tilde{v}(t) \\ dz(t) &= \tilde{C}\eta(t)dt + \tilde{D}d\tilde{v}(t) \end{aligned}$$

where

$$\begin{aligned} \tilde{v}(t) &= \begin{bmatrix} v(t) \\ v_K(t) \end{bmatrix}; \quad \tilde{A} = \begin{bmatrix} A & B_2C_K \\ B_KC_2 & A_K \end{bmatrix}; \\ \tilde{B} &= \begin{bmatrix} B_1 \\ B_KD_{21} \end{bmatrix}; \quad \tilde{G} = \begin{bmatrix} B_0 & B_2B_{K0} \\ B_KD_{20} & B_{K1} \end{bmatrix}; \\ \tilde{C} &= \begin{bmatrix} C_1 & D_{12}C_K \end{bmatrix}; \quad \tilde{D} = \begin{bmatrix} 0 & D_{12}B_{K0} \end{bmatrix}. \end{aligned}$$

Assumptions

1. $D_{12}^T D_{12} = E_1 > 0.$

2. $D_{21} D_{21}^T = E_2 > 0.$

3. The matrix $\begin{bmatrix} A - j\omega I & B_2 \\ C_1 & D_{12} \end{bmatrix}$ is full rank for all $\omega \geq 0.$

4. The matrix $\begin{bmatrix} A - j\omega I & B_1 \\ C_2 & D_{21} \end{bmatrix}$ is full rank for all $\omega \geq 0.$

Riccati Equations

The following Riccati equations will be used to construct the controller:

$$\begin{aligned} (A - B_2 E_1^{-1} D_{12}^T C_1)^T X + X(A - B_2 E_1^{-1} D_{12}^T C_1) \\ + X(B_1 B_1^T - g^2 B_2 E_1^{-1} B_2') X \\ + g^{-2} C_1^T (I - D_{12} E_1^{-1} D_{12}^T) C_1 = 0; \end{aligned}$$

$$\begin{aligned} (A - B_1 D_{21}^T E_2^{-1} C_2) Y + Y(A - B_1 D_{21}^T E_2^{-1} C_2) \\ + Y(g^{-2} C_1^T C_1 - C_2^T E_2^{-1} C_2) Y \\ + B_1 (I - D_{21}^T E_2^{-1} D_{21}) B_1^T = 0. \end{aligned}$$

Controller

The controller matrices A_K , B_K and C_K are determined as follows:

$$A_K = A + B_2 C_K - B_K C_2 + (B_1 - B_K D_{21}) B_1^T X;$$

$$B_K = (I - YX)^{-1} (Y C_2^T + B_1 D_{21}^T) E_2^{-1};$$

$$C_K = -E_1^{-1} (g^2 B_2^T X + D_{12}^T C_1).$$

The remaining controller matrices B_{K0} , B_{K1} and any required noise sources v_K will be discussed below.

Theorem

Necessity. *If there exists a controller of the above form such that the resulting closed loop system is strictly bounded real with disturbance attenuation g , then the above Riccati equations will have solutions $X \geq 0$ and $Y \geq 0$ satisfying*

1. $A - B_2 E_1^{-1} D_{12}^T C_1 + (B_1 B_1^T - g^2 B_2 E_1^{-1} B_2') X$ is a stability matrix.
2. $A - B_1 D_{21}^T E_2^{-1} C_2 + Y (g^{-2} C_1^T C_1 - C_2^T E_2^{-1} C_2)$ is a stability matrix.
3. The matrix XY has a spectral radius strictly less than one.

Sufficiency. Suppose the Riccati equations have solutions $X \geq 0$ and $Y \geq 0$ satisfying

1. $A - B_2 E_1^{-1} D_{12}^T C_1 + (B_1 B_1^T - g^2 B_2 E_1^{-1} B_2') X$ is a stability matrix.
2. $A - B_1 D_{21}^T E_2^{-1} C_2 + Y(g^{-2} C_1^T C_1 - C_2^T E_2^{-1} C_2)$ is a stability matrix.
3. The matrix XY has a spectral radius strictly less than one.

If the controller is such that the matrices A_K, B_K, C_K are given by

$$\begin{aligned} A_K &= A + B_2 C_K - B_K C_2 + (B_1 - B_K D_{21}) B_1^T X; \\ B_K &= (I - YX)^{-1} (Y C_2^T + B_1 D_{21}^T) E_2^{-1}; \\ C_K &= -E_1^{-1} (g^2 B_2^T X + D_{12}^T C_1). \end{aligned}$$

then the resulting closed loop system will be strictly bounded real with disturbance attenuation g .

Physical Realization

Consider the case of a fully quantum controller, of dimension $n = \dim x = \dim \xi$ (even), and no classical degrees of freedom. We take

$$C^{\xi\xi} = 2i \text{diag}(J, \dots, J),$$

an $n \times n$ matrix, where

$$J = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

The input and output channels are also fully quantum, with

$$\begin{aligned} F_y &= I + i \text{diag}(J, \dots, J) \\ F_u &= I + i \text{diag}(J, \dots, J) \\ F_{v_K} &= I + i \text{diag}(J, \dots, J) \end{aligned}$$

We seek a Hamiltonian

$$H_{controller} = \frac{1}{2} \xi^T R \xi$$

and coupling operator vector

$$L_{controller} = \Lambda \xi$$

Here, the matrices $R \geq 0$ and Λ are to be determined and compatible with the controller matrices A_K , B_K and C_K given above.

General form

Edwards-Belavkin, 2005

$$d\xi = -iC^{\xi\xi}(R + \Im(\Lambda^\dagger \Lambda))\xi dt + C^{\xi\xi} \begin{bmatrix} -\Lambda^\dagger & \Lambda^T \end{bmatrix} \Gamma \begin{bmatrix} dv_K \\ dy \end{bmatrix}$$

$$du = P_{N_q^u}^T \begin{bmatrix} \Sigma & 0 \\ 0 & \Sigma \end{bmatrix} \left(\begin{bmatrix} \Lambda + \Lambda^* \\ -i\Lambda + i\Lambda^* \end{bmatrix} \xi dt + P_{n_c} \begin{bmatrix} dv_K \\ dy \end{bmatrix} \right)$$

$$\Sigma = \begin{bmatrix} I_{N_q^u \times N_q^u} & 0_{N_q^u \times (n_c - N_q^u)} \end{bmatrix}.$$

The basic idea is to add additional noise channels to ensure the commutation relations are preserved.

Theorem

The controller is fully quantum realizable if and only if

$$iC^{\xi\xi}A_K + iA_K^T(C^{\xi\xi})^T \geq 0$$

Furthermore, if this condition is satisfied then explicit formulas exist (omitted).

Robust Stability

- [The strict bounded real property of the closed loop system obtained above guarantees stability robustness against real parameter uncertainties.
- [We regard the true physical system as a perturbation of the nominal system used for design.

We suppose that the true closed loop quantum system is described by the equations

$$d\eta(t) = \bar{A}\eta(t)dt + \tilde{G}d\tilde{v}(t)$$

where $\bar{A} = \tilde{A} + \tilde{B}\Delta\tilde{C}$ and Δ is a constant matrix satisfying

$$\Delta^T \Delta \leq I.$$

This closed loop quantum system is said to be *mean square stable* if there exists a real positive definite matrix $X > 0$ and a constant $\lambda > 0$ such that

$$\langle \eta(t)^T X \eta(t) \rangle + \int_0^t \langle \eta(s)^T \eta(s) \rangle ds \leq \langle \eta(0)^T X \eta(0) \rangle + \lambda t \quad \forall t > 0$$

for all Gaussian ρ .

Lemma

The closed loop system is mean square stable if and only if the matrix \bar{A} is asymptotically stable.

Proof: Uses above dissipation results and standard Lyapunov results.

Theorem

*If the **nominal** closed loop system is strictly bounded real then the **true** closed loop system is mean square stable for all Δ satisfying*

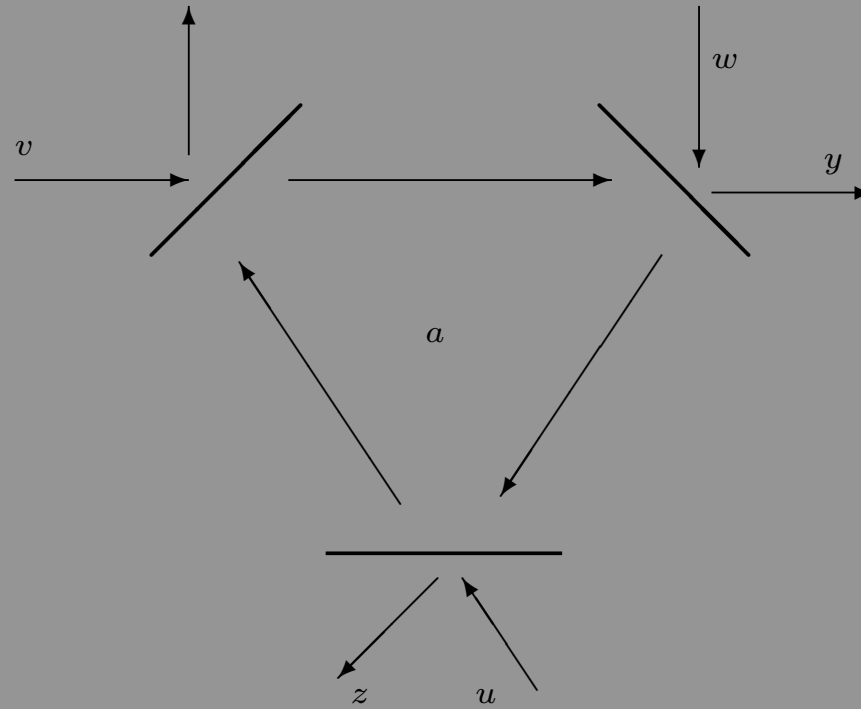
$$\Delta^T \Delta \leq I.$$

Proof: Uses above lemma and standard small gain theorem.

Examples from Quantum Optics

- [H-infinity: Quantum controller
- [H-infinity: Classical controller
- [Robust stability: parameter uncertainty

Plant



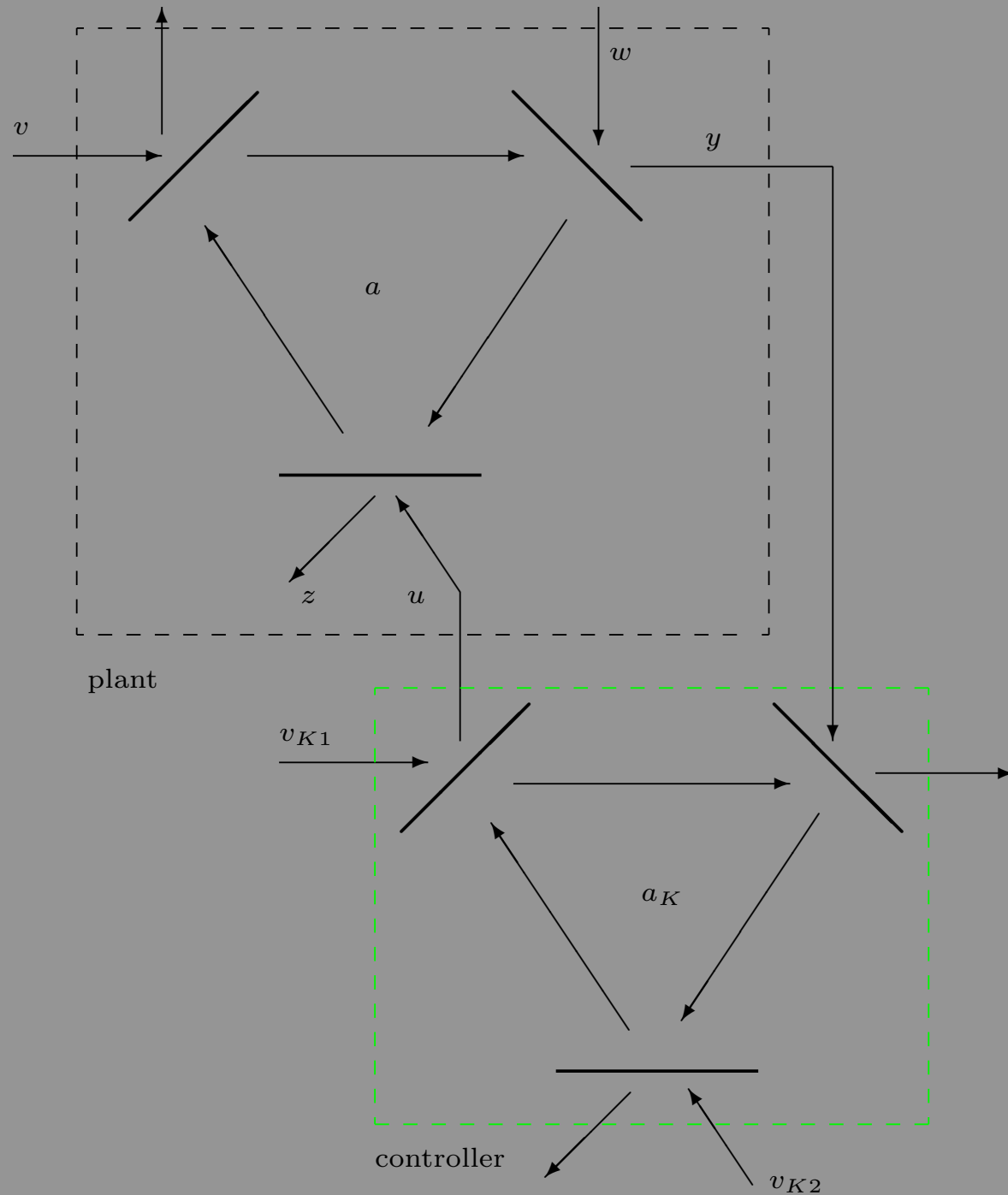
$$da = -\frac{\gamma}{2}adt - \sqrt{\kappa}dV - \sqrt{\kappa}dW - \sqrt{\kappa}dU$$

$$dZ = \sqrt{\kappa}adt + dU$$

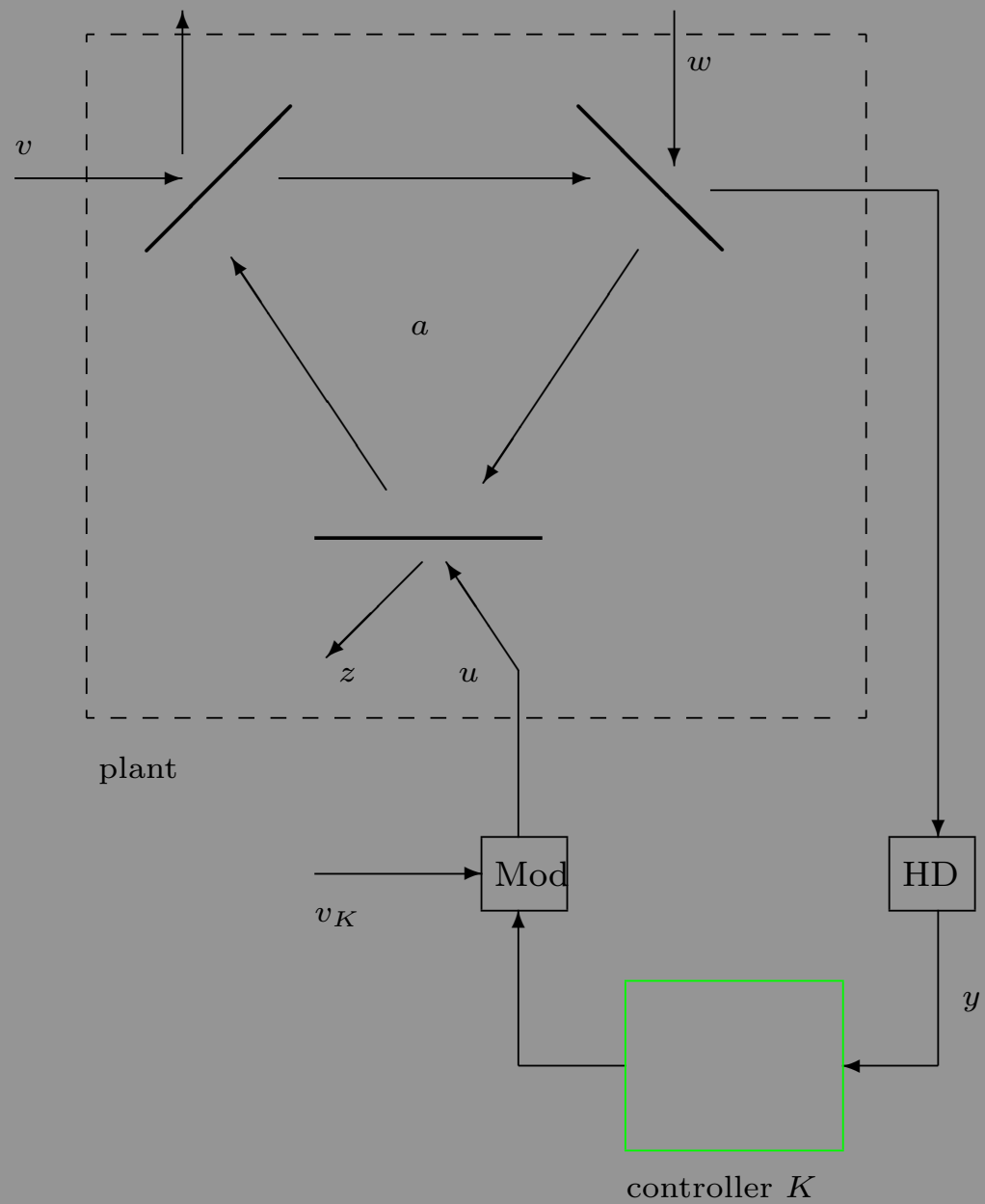
$$dY = \sqrt{\kappa}adt + dW \quad (\text{quantum output})$$

$$dY = \sqrt{\kappa}(a + a^*)dt + d\tilde{w}_1 \quad (\text{classical output})$$

Closed loop with quantum controller



Closed loop with classical controller



Plant with parameter uncertainty

$$\begin{aligned}da &= -\frac{\gamma + \delta}{2}adt - \sqrt{\kappa + \delta}dV - \sqrt{\kappa}dW - \sqrt{\kappa}dU \\dZ &= \sqrt{\kappa}adt + dU \\dY &= \sqrt{\kappa}adt + dW.\end{aligned}$$

where δ is a constant but unknown uncertain parameter satisfying a known bound

$$|\delta| \leq \mu$$

To apply the robust stability results, we write

$$A = -\frac{\gamma}{2}I + \tilde{B}_1\Delta\tilde{C}_1 \text{ where } \tilde{B}_1 = \frac{\mu}{2}, \quad \tilde{C}_1 = T^{-1}$$

and T is any non-singular matrix.

Then

$$\Delta = \frac{\delta}{\mu}I \implies \Delta^T\Delta \leq I$$

and robust stability will follow.

Conclusions

- [We have extended standard methods of H -infinity robust control to the domain of linear quantum systems
- [The controllers may be quantum or classical
- [There are interesting new realization questions
- [The results provide the beginnings of useful robust control design methods for quantum technology