

# Linear Pushbroom Cameras\*

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\*The research described in this paper has been supported by DARPA Contract #MDA972-91-C-0053.

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Figure 1: The pushbroom principle.

## 1 Real Pushbroom Sensors

Fig. 1 shows the idea behind a pushbroom sensor. In general terms, a pushbroom camera consists of an optical system projecting an image onto a linear array of sensors, typically a CCD array. At any time only those points are imaged that lie in the plane defined by the optical center and the line containing the sensor array. This plane will be called the instantaneous view plane or simply *view plane*.

The pushbroom sensor is mounted on a moving platform. As the platform moves, the view plane sweeps out a region of space. The sensor array, and hence the view plane, is approximately perpendicular to the direction of motion. The magnitude of the charge accumulated by each detector cell during some fixed interval, called the *dwell time*, gives the value of the pixel at that location. Thus, at regular intervals of time 1-dimensional images of the view plane are captured. The ensemble of these 1-dimensional images constitutes a 2-dimensional image.

Many times, the camera has no moving parts in it. This fact, which contributes significantly to the superior internal geometric quality of the image, implies that one of the image dimensions depends solely on the sensor motion.

Pushbroom sensors are commonly used in satellite cameras for the generation of 2-D images of the earth's surface. Even though the word "pushbroom camera" is most prevalent in the parlance of remote sensing where it is used to describe a specific type of satellite-mounted camera, the image acquisition principle outlined above is applicable to many other imaging situations. For example, the images acquired by side-looking airborne radar (SLAR), certain types of CT projections, and images in many X-ray metrology setups can all be modeled as pushbroom images. Before going on to a formalization of this model, we briefly outline two real applications of pushbroom imaging.

**SPOT Imagery.** SPOT satellite's HRV camera is a well-known example of a pushbroom system. For SPOT, the linear array of sensors consists of 6000 pixel array of electronic

sensors covering an angle of 4.2 degrees. This sensor array captures a row imagery at 1.504 ms time intervals (i.e. dwell time = 1.504 ms). As the satellite orbits the earth, a continuous strip of imagery is produced. This strip is split into images, each consisting of 6000 rows. Hence a  $6000 \times 6000$  pixel image is captured over a 9 seconds flight of the satellite. Such an image covers a square with side approximately 60 Km on the ground.

The task of modeling an orbiting pushbroom camera exactly is somewhat complex and several factors must be taken into account.

- By Kepler's Laws, the satellite is moving in an elliptical orbit with the center of the earth at one of the foci of the ellipse. The speed is not constant, but varies according to the position of the satellite in its orbit.
- The earth is rotating with respect to the orbital plane of the satellite, so the motion of the satellite with respect to the earth's surface is quite complex.
- The satellite is slowly rotating so that it is approximately fixed with respect to an orthogonal coordinate frame defined as follows: the  $z$ -axis emanate from the satellite and passes through the center of the earth; the  $x$ -axis lies in the plane defined by the satellite velocity vector and the  $z$  axis; the  $y$ -axis is perpendicular to the  $x$  and  $z$  axes. This coordinate frame will be called the *local orbital frame*. During one orbit, the local orbital frame undergoes a complete revolution about its  $y$  axis.
- The orientation of the satellite undergoes slight variations with respect to the local orbital frame.
- The orientation of the view plane with respect to the satellite may not be known.

Some of the parameters of the satellite motion depend on fixed physical and astronomical constants (for example, gravitational constant, mass of the earth, rotational period of the earth). Other parameters such as the major and minor axes and orientation of the satellite orbit are provided as *ephemeris* data with most images. In addition, the fluctuations of the satellite orientation with respect to the local orbital frame are provided as is also the orientation of the view plane. Nevertheless, it has proven necessary for the sake of greater accuracy to refine the ephemeris data by the use of ground-control points.

Even if the orbit of the satellite is known exactly, the task of finding the image coordinates of a point in space is relatively complex. There is no closed-form expression determining the time when the orbiting satellite will pass through a given point in its orbit (time to perigee) — it is necessary to use either an approximation or an iterative scheme. Furthermore the task of determining at what time instant a given ground point will be imaged must be solved by an iterative procedure, such as Newton's method. This means that exact computation of the image produced by a pushbroom sensor is time consuming.

**X-Ray Metrology.** In the most common form of X-ray imagers used for X-ray metrology or part inspection, the object to be viewed is interposed between a point X-ray source and

a linear array of detectors. As the object is moved perpendicular to the fan beam of X-rays, a 2-D image consisting of several 1-D projections is collected. Each image collected in this manner can be treated as a pushbroom image which is orthographic in the direction of motion and perspective in the orthogonal direction (see [?] for details).

## 1.1 Overview

In this paper, a linear approximation to the pushbroom model is introduced. This new model very greatly simplifies the computations involved in working with pushbroom images. The key simplifying assumptions made in deriving this camera model are: (1) the sensor array is traveling in a straight line, and (2) its orientation is constant over the image acquisition duration.

Section 2 defines the linear pushbroom model and derives its basic mathematical form. We will show that under the above assumptions — just as with a pin-hole camera — a *linear pushbroom camera* can be represented by a  $3 \times 4$  camera matrix  $M$ . However, unlike frame cameras,  $M$  represents a non-linear Cremona transformation of object space into image space. In subsequent sections, many of the standard photogrammetric problems associated with parameter determination are solved for the linear pushbroom model. In particular, a linear technique for computing  $M$  from a set of ground control points is described in Section 3. Section 4 describes a method of retrieving camera parameters from  $M$ . All the algorithms discussed are non-iterative, relatively simple, very fast, and do not rely on any extraneous information. This contrasts with parameter determination for the full pushbroom model for satellite cameras, which is slow and requires knowledge of orbital and ephemeris parameters.

Apart from computational efficiency, the linear pushbroom model provides a basis for the mathematical analysis of pushbroom images. The full pushbroom model is somewhat intractable as far as analysis is concerned. On the other hand, the agreement between the full pushbroom model and the linear pushbroom model is so close that results of analyzing the linear pushbroom model will be closely applicable to the full model as well.

An important result derived in this paper concerns the relationship of an image point  $(u_i, v_i)^T$  in the first image with its corresponding point  $(u'_i, v'_i)^T$  in the second image (Section 5). We show that a matrix analogous to the essential matrix for pin-hole cameras ([?, ?, ?]) exists for linear pushbroom cameras as well. In particular, we prove that there exists a  $4 \times 4$  matrix  $Q$ , dubbed *hyperbolic essential matrix*, such that  $(u'_i, u'_i v'_i, v'_i, 1)^T Q (u_i, u_i v_i, v_i, 1) = 0$  for all  $i$ . We also describe a non-iterative technique for deriving  $Q$  from a set of image to image correspondences.

As an example of the theoretical and practical gains achieved by studying the linear pushbroom model is Theorem 5.4 of this paper, which shows that two linear pushbroom views of a generic scene determine the scene up to an affine transformation. This has the practical consequence that affine invariants of a scene may be computed from two pushbroom views. As was shown in [?, ?], a similar result applies to perspective views where the scene is determined up to projectivity from two views. It is hoped that the linear pushbroom model may provide the basis for the development of further image understanding algorithms in the same

way that the pinhole camera model has given rise to a wealth of theory and algorithms.

The results described in this paper can be used to formulate a complete methodology for stereo information extraction from a set of two or more images of a scene acquired via linear pushbroom sensors. In this methodology, which is described in Section 6, no information concerning the relative or absolute orientation and path of the sensors with respect to each other is required. Using a few ground control points, and without resorting to any iterative methods, one can assign 3-D coordinates to a set of image to image correspondences.

One can question the assumptions underlying the linear pushbroom model when used for satellite imagery because the sensor array negotiates an elliptical trajectory and its look direction slowly rotates. However, if the segment of the orbit over which the image was acquired is small, it can be approximated by a straight line. For large orbital segments, one can solve the problem in a piece-wise linear manner. In a final section, the accuracy of the linear pushbroom model is discussed, and the results of some of the algorithms described here are given.

Experimental results confirm that the assumption about linearity is quite valid even for low-earth orbits and it does not have an adverse effect on the accuracy. For example, for SPOT images of size  $6000 \times 6000$  pixels, covering an area about  $60 \times 60$  Km<sup>2</sup>, the linear and full models agree within less than half a pixel. This corresponds to a difference of about  $6 \times 10^{-6}$  radians, or about 5 meters on the ground. Section 7 also presents experimental results that compare the linear pushbroom model with a simple pin-hole camera, and an exact, orbiting pushbroom model that does not make any simplifying assumptions.

## 2 Linear Pushbroom Sensors

In order to simplify the pushbroom camera model to facilitate computation and to provide a basis for theoretical investigation of the pushbroom model, certain simplifying assumptions can be made, as follows.

- The platform is moving in a straight line at constant velocity with respect to the world.
- The orientation of the camera, and hence the view plane, is constant.

This camera can be thought of as a pin-hole camera moving along a linear trajectory in space with constant velocity and fixed orientation (see Fig. 2). Furthermore, the camera is constrained so that at any moment in time it images only points lying in one plane, called the view plane, passing through the center of the camera. Thus, at any moment of time, a 2-dimensional projection of the view plane onto an image line takes place. The orientation of the view plane is fixed, and it is assumed that the motion of the camera does not lie in the view plane. Consequently, the view plane sweeps out the whole of space as time varies between  $-\infty$  and  $\infty$ . The image of an arbitrary point  $\mathbf{x}$  in space is described by two coordinates. The first coordinate  $u$  represents the time when the point  $\mathbf{x}$  is imaged (that is, lies in the view plane) and the second coordinate  $v$  represents the projection of the point on the image line.

Figure 2: Acquisition geometry of a linear pushbroom camera.

We consider an orthogonal coordinate frame attached to the moving camera as follows (see Fig. 2). The origin of the coordinate system is the center of projection. The  $y$  axis lies in the view-plane parallel with the focal plane (in this case, the linear sensor array). The  $z$  axis lies in the view plane perpendicular to the  $y$  axis and directed so that the visible points have positive  $z$  coordinate. The  $x$  coordinate is perpendicular to the view plane such that  $x$ ,  $y$ , and  $z$  axes form a right-handed coordinate frame. The ambiguity of orientation of the  $y$  axis in the above description can be resolved by requiring that the motion of the camera has a positive  $x$  component.

First of all, we consider two dimensional projection. If the coordinates of a point are  $(0, y, z)$  with respect to the camera frame, then the coordinate of this point in the 1-dimensional projection will be  $v = fy/z + p_v$  where  $f$  is the focal length (or magnification) of the camera and  $p_v$  is the principal point offset in the  $v$  direction. This equation may be written in the form

$$\begin{pmatrix} wv \\ w \end{pmatrix} = \begin{pmatrix} f & p_v \\ 0 & 1 \end{pmatrix} \begin{pmatrix} y \\ z \end{pmatrix} \quad (1)$$

where  $w$  is a scale factor (actually equal to  $z$ ).

Now for convenience, instead of considering a stationary world and a moving camera, it will be assumed that the camera is fixed and that the world is moving. A point in space will be represented as  $\mathbf{x}(t) = (x(t), y(t), z(t))^T$  where  $t$  denotes time. Let the velocity vector of the points with respect to the camera frame be  $-\mathbf{V} = -(V_x, V_y, V_z)^T$ . The minus sign is chosen so that the velocity of the camera with respect to the world is  $\mathbf{V}$ . Suppose that a moving point in space crosses the view plane at time  $t_{\text{im}}$  at position  $(0, y_{\text{im}}, z_{\text{im}})^T$ . In the 2-dimensional pushbroom image, this point will be imaged at location  $(u, v)$  where  $u = t_{\text{im}}$  and  $v$  may be expressed using (1). This may be expressed in an equation

$$\begin{pmatrix} u \\ wv \\ w \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & f & p_v \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} t_{\text{im}} \\ y_{\text{im}} \\ z_{\text{im}} \end{pmatrix} \quad (2)$$

Since all points are moving with the same velocity, the coordinates of an arbitrary point  $\mathbf{x}_0$ , as a function of time, are given by the following equation.

$$\mathbf{x}(t) = \mathbf{x}_0 - t\mathbf{V} = (x_0, y_0, z_0)^\top - t(V_x, V_y, V_z) \quad (3)$$

Since the view plane is the plane  $x = 0$ , the time  $t_{\text{im}}$  when the point  $\mathbf{x}$  crosses the view plane is given by  $t_{\text{im}} = x_0/V_x$ . At that moment, the point will be at position

$$(0, y_{\text{im}}, z_{\text{im}})^\top = (0, y_0 - x_0V_y/V_x, z_0 - x_0V_z/V_x)^\top.$$

We may write this as

$$\begin{pmatrix} t_{\text{im}} \\ y_{\text{im}} \\ z_{\text{im}} \end{pmatrix} = \begin{pmatrix} 1/V_x & 0 & 0 \\ -V_y/V_x & 1 & 0 \\ -V_z/V_x & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix} \quad (4)$$

Combining this with (2) gives the equation

$$\begin{pmatrix} u \\ wv \\ w \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & f & p_v \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1/V_x & 0 & 0 \\ -V_y/V_x & 1 & 0 \\ -V_z/V_x & 0 & 1 \end{pmatrix} \begin{pmatrix} x_0 \\ y_0 \\ z_0 \end{pmatrix} \quad (5)$$

Here,  $(x_0, y_0, z_0)^\top$  are the coordinates of the point  $\mathbf{x}$  in terms of the camera frame at time  $t = 0$ . Normally, however, the coordinates of a point are known not in terms of the camera-based coordinate system, but rather in terms of some fixed external orthogonal coordinate system. In particular, let the coordinates of the point in such a coordinate system be  $(x, y, z)^\top$ . Since both coordinate frames are orthogonal, the coordinates are related via a transformation

$$\begin{aligned} (x_0, y_0, z_0)^\top &= R \left( (x, y, z)^\top - (T_x, T_y, T_z)^\top \right) \\ &= (R \mid -R\mathbf{T})(x, y, z, 1)^\top \end{aligned} \quad (6)$$

where  $\mathbf{T} = (T_x, T_y, T_z)^\top$  is the location of the camera at time  $t = 0$  in the external coordinate frame, and  $R$  is a rotation matrix.

Finally, putting this together with (5) leads to

$$\begin{aligned} \begin{pmatrix} u \\ wv \\ w \end{pmatrix} &= \begin{pmatrix} 1 & 0 & 0 \\ 0 & f & p_v \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1/V_x & 0 & 0 \\ -V_y/V_x & 1 & 0 \\ -V_z/V_x & 0 & 1 \end{pmatrix} (R \mid -R\mathbf{T}) \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix} \\ &= M(x, y, z, 1)^\top \end{aligned} \quad (7)$$

Eq. (7) should be compared with the basic equation describing pinhole, or perspective cameras, namely  $(wu, wv, w)^\top = M(x, y, z, 1)^\top$  where  $(x, y, z)^\top$  are the coordinates of a world point,  $(u, v)^\top$  are the coordinates of the corresponding image point and  $w$  is a scale factor. It may be seen that a linear pushbroom image may be thought of as a projective image in one direction (the  $v$  direction) and an orthographic image in the other direction (the  $u$  direction).

The camera matrix  $M$  in Eq. (7) for a linear pushbroom sensor can model translation, rotation, and scaling of the 3-D world coordinates as well as translation and scaling of 2-D image coordinates. However, it cannot account for rotation in the image plane. In general, a 2-D perspective transform of an image taken by a linear pushbroom camera cannot be thought of as another image taken by different linear pushbroom camera. Many resampling operation — e.g. resampling images in a stereo pair so that the match point disparities are only along one of the image coordinates [?] — cannot be performed on linear pushbroom imagery without breaking the mapping encoded in Eq. (7).

### 3 Determination of the Camera Matrix

In this section it will be shown how a linear pushbroom camera matrix may be computed given a set of ground control points. The method is an adaptation of the method of Roberts or Sutherland ([?]) used for the pinhole cameras. In particular, denoting by  $\mathbf{m}_1^\top$ ,  $\mathbf{m}_2^\top$  and  $\mathbf{m}_3^\top$  the three rows of the matrix  $M$  and  $\mathbf{x} = (x, y, z, 1)^\top$  a ground control point, (7) may be written in the form of three equations

$$\begin{aligned} u &= \mathbf{m}_1^\top \mathbf{x} \\ wv &= \mathbf{m}_2^\top \mathbf{x} \\ w &= \mathbf{m}_3^\top \mathbf{x} . \end{aligned} \tag{8}$$

The unknown factor  $w$  can be eliminated leading to two equations

$$\begin{aligned} u &= \mathbf{m}_1^\top \mathbf{x} \\ v\mathbf{m}_3^\top \mathbf{x} &= \mathbf{m}_2^\top \mathbf{x} \end{aligned} \tag{9}$$

Supposing that the world coordinates  $(x, y, z)$  and image coordinates  $(u, v)$  are known, equations (9) are a set of linear equations in the unknown entries of the matrix  $M$ . Given sufficient ground control points we can solve for the matrix  $M$ . Note that the entries in the row  $\mathbf{m}_1^\top$  rely only on the  $u$  coordinates of the ground control points. Given four ground control points, we can solve for the first row of  $M$ . Similarly, the second and third rows of  $M$  depend only on the  $v$  coordinates of the matrix. Given five ground control points we can solve for the second and third rows of  $M$  up to the undetermined factor. With more ground control points, linear least squares solutions methods can be used to determine the best solution.

This linear technique for camera model estimation should be contrasted with other satellite camera models described in the literature (see, for example, [?, ?]). Most traditional models for satellite cameras typically simulates the complex orbital geometry and imaging conditions to map object space points to image coordinates. The resulting non-linear equations in model parameters can only be solved using iterative methods as purely non-iterative methods — e.g. those by Sutherland [?] or Longuet-Higgins [?] in the realm of pinhole cameras — are unavailable.

**Mapping of Lines under  $M$ .** In order to see the non-linear nature of the mapping function performed by  $M$ , it is instructive to see how lines in space are mapped in the image plane by  $M$ . A linear pushbroom transforms a point  $\mathbf{x}$  in to  $u$  and  $v$  according to Eq. 9. Constraining  $\mathbf{x}$  to lie on a line in 3-D is given by  $V_p + tV_a$ , where  $V_p$  is a point on the line, and  $V_a$  is a vector along the line, the image of this line under  $M$  is given by

$$u = \mathbf{m}_1^\top (V_p + tV_a) \quad (10)$$

$$v = \frac{\mathbf{m}_2^\top (V_p + tV_a)}{\mathbf{m}_3^\top (V_p + tV_a)} \quad (11)$$

Eliminating  $t$  from these equations, one gets an equation of the form  $\alpha u + \beta v + \gamma uv + \delta = 0$ , which is the equation of a hyperbola in the image plane.

## 4 Parameter Retrieval

It may be seen that the last two rows of matrix  $M$  may be multiplied by a constant without affecting the relationship between world point coordinates  $(x, y, z)$  and image coordinates  $(u, v)$  expressed by (7). This means that the  $3 \times 4$  matrix  $M$  contains only 11 degrees of freedom. On the other hand, it may be verified that the formation of a linear pushbroom image is also described by 11 parameters, namely the position (3) and orientation (3) of the camera at time  $t=0$ , the velocity of the camera (3) and the focal length and v-offset (2). It will next be shown how the linear pushbroom parameters may be computed given the matrix  $M$ . This comes down to finding a factorization of  $M$  of the kind given in (7). The corresponding problem for pinhole cameras has been solved by Ganapathy ([?]) and Strat ([?]).

First of all we determine the position of the camera at time  $t = 0$ , referred to subsequently as the initial position of the camera. Multiplying out the product (7) it may be seen that  $M$  is of the form  $(K \mid -K\mathbf{T})$  for a non-singular  $3 \times 3$  matrix  $K$ . Therefore, it is easy to solve for  $\mathbf{T}$  by solving the linear equations  $K\mathbf{T} = -\mathbf{c}_4$  where  $\mathbf{c}_4$  is the last column of  $M$ , and  $K$  is the left-hand  $3 \times 3$  block.

Next, we consider the matrix  $K$ . According to (7), and bearing in mind that the two bottom rows of  $K$  may be multiplied by a constant factor  $k$ , matrix  $K$  is of the form

$$K = \begin{pmatrix} 1/V_x & 0 & 0 \\ -k(fV_y/V_x + p_v V_z/V_x) & kf & kp_v \\ -kV_z/V_x & 0 & k \end{pmatrix} R \quad (12)$$

where  $R$  is a rotation matrix. In order to find this factorization, we may multiply  $K$  on the right by a sequence of rotation matrices to reduce it to the form of the left hand factor in (12). The necessary rotations will be successive Givens rotations about the  $z$ ,  $y$  and  $x$  axes with angles chosen to eliminate the (1,2), (1,3) and (3,2) entries of  $K$ . In this way, we find a factorization of  $K$  as a product  $K = LR$  where  $R$  is a rotation matrix and  $L$  is a matrix having zeros in the required positions. It is not hard to verify that such a factorization is unique. Equating  $L$  with the left hand matrix in (12) it is seen that the parameters  $f$ ,  $p_v$ ,  $V_x$ ,  $V_y$  and  $V_z$  may easily be read from the matrix  $L$ . In summary

**Proposition 4.1.** *The 11 parameters of a linear pushbroom camera are uniquely determined and may be computed from the  $3 \times 4$  camera matrix.*

## 5 Relative Camera Model Determination

The problem of determining the relative camera placement of two or more pinhole cameras and consequent determination of pinhole cameras has been extensively considered. Most relevant to the present paper is the work of Longuet-Higgins ([?]) who introduced the so-called essential matrix  $Q$ . If  $\{(\tilde{u}_i, \tilde{u}'_i)\}$  is a set of match points in a stereo pair,  $Q$  is defined by the relation  $\tilde{u}'_i{}^T Q \tilde{u}_i = 0$  for all  $i$ . As shown in [?],  $(r, s, t)^T = Q \tilde{u}_i$  is the equation of the epipolar line corresponding to  $\tilde{u}_i$ , in the second image. (The line  $(r, s, t)^T$  in homogeneous coordinates corresponds to the line equation  $ru + sv + t = 0$ , in the image-space.)  $Q$  may be determined from eight or more correspondence points between two images by linear techniques.

Other non-linear techniques for determining  $Q$ , more stable in the presence of noise, have been published ([?, ?, ?, ?]). Those techniques relate especially to so called “calibrated cameras”, for which the internal parameters are known. A paper that deals with the determination of the essential matrix for uncalibrated cameras is [?]. As for the determination of the world coordinates of points seen from two pinhole cameras, it has been shown ([?, ?]) that for uncalibrated cameras the position of world points is determined up to an unknown projective transform by their images in two separate views.

Similar results for linear pushbroom cameras will be shown here. In Section 5.1, the *hyperbolic essential matrix* for linear pushbroom cameras, which is analogous to the essential matrix for pinhole cameras, is introduced. The epipolar geometry of linear pushbroom cameras is discussed in Section 5.2. In Section 5.3, we prove that a hyperbolic essential matrix, which encodes the relative orientation of two linear pushbroom cameras, determines the 3-D points in object space up to an affine transformation of space. Thus the knowledge of relative orientation in the case of linear pushbrooms is more constraining than that for the pin-hole cameras; in the later case the ambiguity is a projective transformation of space. Sections 5.4 and 5.5 are devoted to a discussion of the critical sets and computation of  $Q$  from a set of match points.

### 5.1 Definition of Hyperbolic Essential Matrix

Consider a point  $\mathbf{x} = (x, y, z)^T$  in space as viewed by two linear pushbroom cameras with camera matrices  $M$  and  $M'$ . Let the images of the two points be  $\mathbf{u} = (u, v)^T$  and  $\mathbf{u}' = (u', v')^T$ . This gives a pair of equations

$$\begin{aligned} (u, wv, w)^T &= M(x, y, z, 1)^T \\ (u', w'v', w')^T &= M'(x, y, z, 1)^T \end{aligned} \tag{13}$$

This pair of equations may be written in a different form as

$$\begin{pmatrix} m_{11} & m_{12} & m_{13} & m_{14} - u & 0 & 0 \\ m_{21} & m_{22} & m_{23} & m_{24} & v & 0 \\ m_{31} & m_{32} & m_{33} & m_{34} & 1 & 0 \\ m'_{11} & m'_{12} & m'_{13} & m'_{14} - u' & 0 & 0 \\ m'_{21} & m'_{22} & m'_{23} & m'_{24} & 0 & v' \\ m'_{31} & m'_{32} & m'_{33} & m'_{34} & 0 & 1 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \\ 1 \\ w \\ w' \end{pmatrix} = 0 \quad (14)$$

The  $6 \times 6$  matrix in (14) will be denoted  $A(M, M')$ . Considered as a set of linear equations in the variables  $x, y, z, w$  and  $w'$  and constant 1, this is a set of six homogeneous equations in six unknowns (imagining 1 to be an unknown). If this system is to have a solution, then  $\det A(M, M') = 0$ . This condition gives rise to a cubic equation  $p(u, v, u', v') = 0$  where the coefficients of  $p$  are determined by the entries of  $M$  and  $M'$ . The polynomial  $p$  will be called the *essential polynomial* corresponding to the two cameras. Because of the particular form of  $p$ , there exists a  $4 \times 4$  matrix  $Q$  such that

$$(u', u'v', v', 1)Q(u, uv, v, 1)^T = 0 \quad (15)$$

The matrix  $Q$  will be called the *hyperbolic essential matrix* corresponding to the linear pushbroom camera pair  $\{M, M'\}$ . Matrix  $Q$  is just a convenient way to display the coefficients of the essential polynomial. Since the entries of  $Q$  depend only on the two camera matrices,  $M$  and  $M'$ , equation (15) must be satisfied by any pair of corresponding image points  $(u, v)$  and  $(u', v')$ .

It is seen that if either  $M$  or  $M'$  is replaced by an equivalent matrix by multiplying the last two rows by a constant  $c$ , then the effect is to multiply  $\det A(M, M')$ , and hence the fundamental polynomial  $p$  and matrix  $Q$  by the same constant  $c$  (not  $c^2$  as may appear at first sight). Consequently, two essential polynomial or matrices that differ by a constant non-zero factor will be considered equivalent. The same basic proof method used above may be used to prove the existence of the essential matrix for pinhole cameras.

A closer examination of the matrix  $A(M, M')$  in (14) reveals that  $p = \det A(M, M')$  contains no terms in  $uu', uvu', uu'v'$  or  $uvu'v'$ . In other words, the top left hand  $2 \times 2$  submatrix of  $Q$  is zero. This is formally stated below.

**Theorem 5.2.** *Let  $\mathbf{u}_i = (u_i, v_i, 1)^T$  and  $\mathbf{u}'_i = (u'_i, v'_i, 1)^T$  be the image coordinates of 3-D points  $p_i$  ( $i = 1 \dots n$ ) under two linear pushbroom cameras. For all  $i$ , there exists a matrix  $Q$ , such that*

$$Q = \begin{pmatrix} u'_i & u'_i v'_i & v'_i & 1 \end{pmatrix} \begin{pmatrix} 0 & 0 & q_{13} & q_{14} \\ 0 & 0 & q_{23} & q_{24} \\ q_{31} & q_{32} & q_{33} & q_{34} \\ q_{41} & q_{42} & q_{43} & q_{44} \end{pmatrix} \begin{pmatrix} u_i \\ u_i v_i \\ v_i \\ 1 \end{pmatrix} = 0. \quad (16)$$

Since  $Q$  is defined only up to a constant factor, it contains no more than 11 degrees of freedom. Given a set of 11 or more image-to-image correspondences the matrix  $Q$  can be determined by the solution of a set of linear equations just as with pinhole cameras.

Figure 3: Epipolar lines

## 5.2 Epipolar Geometry

One of the most striking differences between linear pushbroom and perspective cameras is the epipolar geometry. First of all there are no epipoles in the familiar manner of perspective cameras, since the two pushbroom cameras are moving with respect to each other. Neither is it true that epipolar lines are straight lines.

Consider a pair of matched point  $(u, v)^\top$  and  $(u', v')^\top$  in two images. According to equation (15) these points satisfy  $(u', u'v', v', 1)Q(u, uv, v, 1)^\top = 0$ . Now, fixing  $(u, v)^\top$  and inquiring for the locus of all possible matched points  $(u', v')^\top$ , and writing  $(\alpha, \beta, \gamma, \delta)^\top = Q(u, uv, v, 1)^\top$ , we see that  $\alpha u' + \beta u'v' + \gamma v' + \delta = 0$ . This is the equation of a hyperbola – epipolar loci are hyperbolas for linear pushbroom cameras.  $Q$  can be used in match point computation to enforce the epipolar constraint.

Fig. 3 shows the images of a set of lines in space as taken with a linear pushbroom camera. The curvature of the lines is exaggerated by the wide field of view.

The epipolar locus of a point is the projection in the second image of a straight line emanating from the instantaneous center of projection of the first camera. Hyperbolic epipolar curves are expected because, as already proved, under the linear push-broom model lines in space map into hyperbolas in the image plane. Only one of the two branches of the hyperbola will be visible in the image. The other branch will lie behind the camera.

Hyperbolic essential matrix contains all the information about relative camera parameters for completely *uncalibrated* linear pushbroom cameras (i.e., cameras about which nothing is known) that can be derived from a set of match points. In the following section, we consider the information that can be extracted from  $Q$ .

## 5.3 Extraction of Relative Cameras from $Q$

Longuet-Higgins ([?]) showed that for calibrated cameras the relative position and orientation of the two cameras may be deduced from the essential matrix. This result was extended to uncalibrated cameras in [?] where it was shown that if  $M_1$  and  $M'_1$  are one pair of cameras corresponding to an essential matrix  $Q$  and if  $M_2$  and  $M'_2$  are another pair corresponding

to the same essential matrix, then there is a  $4 \times 4$  matrix  $H$  such that  $M_1 = M_2H$  and  $M'_1 = M'_2H$ . This result will be shown to hold for linear pushbroom cameras with the restriction that  $H$  must be a matrix representing an affine transformation, that is, the last row of  $H$  is  $(0, 0, 0, 1)$ .

First of all, it will be shown that  $M$  and  $M'$  may be multiplied by an arbitrary affine transformation matrix without changing the hyperbolic essential matrix. Let  $H$  be a  $4 \times 4$  affine transformation matrix and let  $\hat{H}$  be the  $6 \times 6$  matrix

$$\hat{H} = \begin{pmatrix} H & 0 \\ 0 & I \end{pmatrix}$$

where  $I$  is the  $2 \times 2$  identity matrix. If  $A$  is the matrix in (14) it may be verified with a little work that  $A(M, M')\hat{H} = A(MH, M'H)$ , where the assumption that the last row of  $H$  is  $(0, 0, 0, 1)$  is necessary. Therefore,  $\det A(MH, M'H) = \det A(M, M') \det H$  and so the fundamental polynomials corresponding to pairs  $\{M, M'\}$  and  $\{MH, M'H\}$  differ by a constant factor and so are equivalent.

Next we will consider to what extent the two camera matrices  $M$  and  $M'$  can be determined from the hyperbolic essential matrix. As has just been demonstrated, they may be multiplied by an arbitrary  $4 \times 4$  affine matrix  $H$ . Therefore, we may choose to set the matrix  $M'$  to a particularly simple form  $(I | 0)$  where  $I$  is an identity matrix, by multiplication of both  $M$  and  $M'$  by the affine matrix  $\begin{pmatrix} M'^{-1} & \mathbf{t} \\ 0 & 1 \end{pmatrix}$ . It will be seen that with the assumption that  $M' = (I | 0)$ , the other matrix  $M$  is almost uniquely determined by the hyperbolic essential matrix.

Under the assumption that  $M' = (I | 0)$ ,  $Q$  may be computed explicitly in terms of the entries of  $M$ . Using Mathematica([?]) or by hand it may be computed that

$$Q = (q_{ij}) = \begin{pmatrix} 0 & 0 & m_{11}m_{33} - m_{13}m_{31} & m_{13}m_{21} - m_{11}m_{23} \\ 0 & 0 & m_{11}m_{32} - m_{12}m_{31} & m_{12}m_{21} - m_{11}m_{22} \\ m_{22} & -m_{32} & m_{14}m_{32} - m_{12}m_{34} & m_{12}m_{24} - m_{14}m_{22} \\ m_{23} & -m_{33} & m_{14}m_{33} - m_{13}m_{34} & m_{13}m_{24} - m_{14}m_{23} \end{pmatrix} \quad (17)$$

Given the entries  $q_{ij}$  of  $Q$  the question is whether it is possible to retrieve the values of the entries  $m_{ij}$ . This involves the solution of a set of 12 equations in the 12 unknown values  $m_{ij}$ . The four entries  $m_{22}$ ,  $m_{23}$ ,  $m_{32}$  and  $m_{33}$  may be immediately obtained from the bottom left hand block of  $Q$ . In particular,

$$\begin{aligned} m_{22} &= q_{31} \\ m_{23} &= q_{41} \\ m_{32} &= -q_{32} \\ m_{33} &= -q_{42} \end{aligned} \quad (18)$$

Retrieval of the remaining entries is more tricky but may be accomplished as follows. The four non-zero entries in the first row can be rewritten in the following form (using (18) to

substitute for  $m_{22}$ ,  $m_{23}$ ,  $m_{32}$  and  $m_{33}$ ).

$$\begin{pmatrix} -q_{42} & 0 & -m_{13} & -q_{13} \\ -q_{41} & m_{13} & 0 & -q_{14} \\ -q_{32} & 0 & -m_{12} & -q_{23} \\ -q_{31} & m_{12} & 0 & -q_{24} \end{pmatrix} \begin{pmatrix} m_{11} \\ m_{21} \\ m_{31} \\ 1 \end{pmatrix} = 0 . \quad (19)$$

Similarly, the bottom right hand  $2 \times 2$  block gives a set of equations

$$\begin{pmatrix} -q_{42} & 0 & -m_{13} & -q_{43} \\ -q_{41} & m_{13} & 0 & -q_{44} \\ -q_{32} & 0 & -m_{12} & -q_{33} \\ -q_{31} & m_{12} & 0 & -q_{34} \end{pmatrix} \begin{pmatrix} m_{14} \\ m_{24} \\ m_{34} \\ 1 \end{pmatrix} = 0 . \quad (20)$$

Immediately it can be seen that if we have a solution  $m_{ij}$ , then a new solution may be obtained by multiplying  $m_{12}$  and  $m_{13}$  by any non-zero constant  $c$  and dividing  $m_{21}$ ,  $m_{31}$ ,  $m_{24}$  and  $m_{34}$  by the same constant  $c$ . In other words, unless  $m_{13} = 0$ , which may easily be checked, we may assume that  $m_{13} = 1$ . From the assumption of a solution to (19) and (20) may be deduced that  $4 \times 4$  matrices in (19) and (20) must both have zero determinant. With  $m_{13} = 1$ , each of (19) and (20) gives a quadratic equation in  $m_{12}$ . In order for a solution to exist for the sought matrix  $M$ , these two quadratics must have a common root. This condition is a necessary condition for a matrix to be a hyperbolic essential matrix. Rearranging the matrices slightly, writing  $\lambda$  instead of  $m_{12}$  and expressing the existence of a common root in terms of the resultant leads to the following statement.

**Theorem 5.3.** *If a matrix  $4 \times 4$  matrix  $Q = (q_{ij})$  is a hyperbolic essential matrix, then*

1.  $q_{11} = q_{12} = q_{21} = q_{22} = 0$
2. *the resultant of the polynomials*

$$\det \begin{pmatrix} \lambda & 0 & q_{31} & q_{24} \\ 0 & \lambda & q_{32} & q_{23} \\ 1 & 0 & q_{41} & q_{14} \\ 0 & 1 & q_{42} & q_{13} \end{pmatrix} \quad (21)$$

*and*

$$\det \begin{pmatrix} \lambda & 0 & q_{31} & q_{34} \\ 0 & \lambda & q_{32} & q_{33} \\ 1 & 0 & q_{41} & q_{44} \\ 0 & 1 & q_{42} & q_{43} \end{pmatrix} \quad (22)$$

*vanishes.*

3. *The discriminants of the polynomials (21) and (22) are both non-negative.*

If the two quadratics have a common root, then this common root will be the value of  $m_{12}$ . The linear equations (19) may then be solved for  $m_{11}$ ,  $m_{21}$  and  $m_{31}$ . Similarly, equations (20) may be solved for  $m_{14}$ ,  $m_{24}$  and  $m_{34}$ . Unless  $q_{31}q_{42} - q_{41}q_{32}$  vanishes, the first three columns of the matrices (21) and (22) will be linearly independent and the solutions for the  $m_{ij}$  will exist and be unique.

To recapitulate, if  $m_{12}$  is a common root of the two quadratic polynomials (21) and (22),  $m_{13}$  is chosen to equal 1, and  $q_{31}q_{42} - q_{41}q_{32} \neq 0$  then the matrix  $M = (m_{ij})$  may be uniquely determined by the solution of a set of linear equations. Relaxing the condition  $m_{13} = 1$ , leads to a family of solutions of the form

$$\begin{pmatrix} m_{11} & m_{12}c & m_{13}c & m_{14} \\ m_{21}/c & m_{22} & m_{23} & m_{24}/c \\ m_{31}/c & m_{32} & m_{33} & m_{34}/c \end{pmatrix} \quad (23)$$

However, up to multiplication by the diagonal affine matrix  $\text{diag}(1, 1/c, 1/c, 1)$  all such matrices are equivalent. Furthermore, the matrix  $M' = (I \mid 0)$  is mapped unto an equivalent matrix by multiplication by  $\text{diag}(1, 1/c, 1/c, 1)$ . This shows that once  $m_{12}$  is determined, the matrix pair  $\{M, M'\}$  may be computed uniquely up to affine equivalence.

Finally, we consider the possibility that the equations (21) and (22) have two common roots. This can only occur if the coefficients of  $Q$  satisfy certain restrictive identities that may be deduced from (21) and (22). This allows us to state

**Theorem 5.4.** *Given a  $4 \times 4$  matrix  $Q$  satisfying the conditions of Proposition 5.3, the pair of camera matrices  $\{M, M'\}$  corresponding to  $Q$  is uniquely determined up to affine equivalence, unless  $Q$  lies in a lower dimensional critical set.*

## 5.4 More about the Critical Set

It is not the purpose here to undertake a complete investigation of the critical set. As previously stated, conditions under which there are two common roots to (21) and (22) leading to two distinct solutions for  $M$  may be deduced from the form of (21) and (22). This investigation will give a condition in terms of the entries of  $Q$ . More enlightening would be a conditions in terms of the entries of the matrix  $M$  for the solution to be ambiguous. This will be investigated next.

There will be ambiguous solutions to the problem of estimating the matrix  $M$  if the polynomials (21) and (22) have two common roots. Suppose that the matrix  $Q$  is of the form given in (17). Then we may compute the two quadratic polynomials from (21) and (22). The results<sup>2</sup> are

$$\begin{aligned} p_1(\lambda) &= (m_{13}\lambda - m_{12})(m_{22}m_{31} - m_{21}m_{32} - \lambda(m_{23}m_{31} - m_{21}m_{33})) \\ p_2(\lambda) &= (m_{13}\lambda - m_{12})(m_{22}m_{34} - m_{24}m_{32} - \lambda(m_{23}m_{34} - m_{24}m_{33})) \end{aligned}$$

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<sup>2</sup>These computations were carried out using Mathematica ([?])

As expected,  $p_1(\lambda)$  and  $p_2(\lambda)$  have a common root  $\lambda = m_{12}/m_{13}$ . The second root of  $p_1$  and  $p_2$  is the same if and only if two linear polynomials  $(m_{22}m_{31} - m_{21}m_{32} - \lambda(m_{23}m_{31} - m_{21}m_{33}))$  and  $(m_{22}m_{34} - m_{24}m_{32} - \lambda(m_{23}m_{34} - m_{24}m_{33}))$  have the same root. This is so if and only if

$$(m_{21}m_{34} - m_{24}m_{31})(m_{22}m_{33} - m_{23}m_{32}) = 0 \quad (24)$$

Since the right hand side of this expression is a product of two factors, there are two separate conditions under which an ambiguous solution exists. The first condition  $(m_{21}m_{34} - m_{24}m_{31}) = 0$  corresponds geometrically to the situation where the trajectories of the two cameras meet in space. This may be seen as follows. A point  $\mathbf{x} = (x, y, z)^\top$  lies on the trajectory of the centre of projection of a camera with matrix  $M$  if and only if  $M(x, y, z, 1)^\top = (u, 0, 0)^\top$ , for under these circumstances the  $v$  coordinate of the image is undefined. In particular, the points that lie on the trajectory of the camera  $M'$  with matrix  $(I \mid 0)$  are of the form  $(x, 0, 0)^\top$ . Such a point will also lie on the trajectory of the camera with matrix  $M$  if and only if  $xm_{21} + m_{24} = xm_{31} + m_{34} = 0$  for some  $x$  – that is, if and only if  $m_{21}m_{34} - m_{24}m_{31} = 0$ .

The geometrical meaning of the other condition has not been determined so far.<sup>3</sup>

## 5.5 Computation of Hyperbolic Essential Matrix

The matrix  $Q$  may be computed from image correspondences in much the same way as Longuet-Higgins computes the perspective essential matrix ([?]). Given 11 or more point-to-point correspondences between a pair of linear pushbroom images, equation (15) can be used to solve for the 12 non-zero entries of  $Q$ , up to multiplication by an unknown scale. Unfortunately, in the presence of noise, the solution found in this way for  $Q$  will not satisfy the second condition of (5.3) exactly. Consequently, when solving for the matrix  $M$ , one will find that the two polynomials (21) and (22) do not have a common root. Various strategies are possible at this stage.

One strategy is as follows. Consider each of the two roots  $m_{12}$  of (21) and with each such value of  $m_{12}$  proceed as follows : Substitute each such  $m_{12}$  in turn into the equation (20). giving a set of four equations in three unknowns; solve (20) to find the least-squares solution for  $m_{14}$ ,  $m_{24}$  and  $m_{34}$ . Finally accept the root of (21) that leads to the best least-squares solution. One could do this the other way round as well starting by considering the roots of (22) and accepting the best of the four solutions found. A different strategy is to choose  $m_{12}$  to be the number that is closest to being a root of each of (21) and (22). This is the algorithm that we have implemented, with good results so far.

To obtain the best results, however, it is probably necessary to take the conditions of Proposition 5.3 into account explicitly and compute a hyperbolic essential matrix satisfying these conditions using explicit assumptions about the source of error to formulate a cost function to be minimized. This has been shown to be the best approach for perspective cameras ([?, ?]).

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<sup>3</sup>The condition seems to be that trajectory of the second camera lies parallel to the view plane of the other camera, but this needs to be checked.

Let us assume that the error is in the specification of the image coordinates  $(u_i, v_i)^\top$  and  $(u'_i, v'_i)^\top$  in the two images, and that the errors in coordinates are independent Gaussian variables. For simplicity we assume that the variances of individual pixels are the same, though this assumption is not necessary. In this case, the correct minimization problem is to find a matrix  $Q$  and coordinates  $(\hat{u}_i, \hat{v}_i)^\top$  and  $(\hat{u}'_i, \hat{v}'_i)^\top$  such that  $Q$  is of the form specified by Proposition 5.3, the epipolar constraint  $(\hat{u}'_i, \hat{u}'_i \hat{v}'_i, \hat{v}'_i, 1)^\top Q(\hat{u}_i, \hat{u}_i \hat{v}_i, \hat{v}_i, 1) = 0$  is satisfied for all  $i$  and the difference  $\sum_i (u_i - \hat{u}_i)^2 + (v_i - \hat{v}_i)^2 + (u'_i - \hat{u}'_i)^2 + (v'_i - \hat{v}'_i)^2$  is minimized. This problem can be solved using a standard photogrammetric resection approach. Instead of solving for  $Q$ , we solve for the camera matrix  $M$  and the world point locations  $\mathbf{x}_i$ . We assume without loss of generality that  $M' = (I \mid 0)$ . Given an estimate for  $M$  and each  $\hat{\mathbf{x}}_i$ , image coordinates  $(\hat{u}_i, \hat{v}_i)^\top$  and  $(\hat{u}'_i, \hat{v}'_i)^\top$  are computed from the basic formula (7) and the cost function to be minimized is the squared pixel error. An initial estimate of the camera matrix  $M$  may be computed using the straight-forward linear approach given above. By non-linear least squared iteration a final estimate for  $M$  and each  $\mathbf{x}_i$  is found. The hyperbolic essential matrix  $Q$  may be computed from the final estimate of  $M$ . Although this method has not been tested on pushbroom cameras, it has proven successful with perspective cameras.

The problem with the above method is that a large non-linear problem must be solved. A comparison of this method and a different, fast and almost optimal method that uses the correlation matrix of  $Q$  may form the subject of another paper.

The question of numerical stability is important in implementing algorithms using the linear pushbroom model. In particular, it is easy to encounter situations in which the determination of the linear pushbroom model parameters is very badly conditioned. In particular, if a set of ground-control points lie in a plane or are very close to being planar, then it is easily seen (just as with perspective cameras) that the determination of the model parameters is ambiguous. We have developed techniques (not described here) for handling some cases of instability, but care is still necessary. The algorithms described in this paper can not be used in cases where the object set lies in a plane.

## 6 Scene Reconstruction

Once two camera matrices have been determined, the position of the points  $\mathbf{x}_i$  in space may be determined by solving (14). This will determine the position of the points in space up to an affine transformation of space.

In the case where both point matches between images and ground-control points are given, the scene may be reconstructed by using the matched points to determine the scene up to affine transformation, and then using the ground-control points to determine the absolute placement of the scene. If the ground control points are visible in both images, then it is easy to find the correct affine transformation. This is done by determining the position of the ground control points in the reconstructed image, and then determining the 3-D affine transformation that will take these points on to the absolute ground-control locations.

If ground-control points are available that are visible in one image only, it is still possible to use them to determine the absolute location of the reconstructed point set. A method for

doing this is given in [?] and will not be repeated here.

## 7 Experimental Results

Two key assumptions are made in the derivation of the linear pushbroom model (ref. section 2). In the context of remote sensing applications, the first assumption is that during the time of acquisition of one image the variations in velocity of the satellite in its orbit are negligible. In addition, the motion of the earth's surface can be included in the motion of satellite, the composite motion being approximately rectilinear. The second assumption is that the rotation of the local orbital frame as well as the fluctuations of orientation with respect to this frame can be ignored. To what extent these assumptions are justified is explored this section and several experiments that measure the accuracy of the linear pushbroom model are described.

In the first experiment, the accuracy of the linear pushbroom model was compared with a full model of SPOT's HRV camera. This model, which is detailed in [?], takes into account the orbital dynamics, earth rotation, attitude drift as measured by on-board systems, ephemeris data, and several other phenomena to emulate the imaging process as accurately as possible. A different model is discussed in [?].

The linear pushbroom model was compared with the full model on a pair of real images with matched points computed using a stereo matching algorithm. A stereo pair of SPOT images of the Malibu region, centered approximately at 34 deg 5 min north, and 118 deg 32 min west (images with  $(J, K) = (541, 281)$  and  $(541, 281)$  in SPOT's grid reference system [?]) were used. We estimated the camera models for these two images using a set of 25 ground control points, visible in both images, picked from USGS maps and several automatically generated image to image correspondences found using STEREOSYS ([?]).

Two performance metrics were computed. The accuracy with which the camera model maps the ground points to their corresponding image points is important. The RMS difference between the known image coordinates and the image coordinates computed using the derived camera models was measured. An application-specific metric, viz. the accuracy of the terrain elevation model generated from a stereo pair, was also measured.

Once again, the data was modeled using a perspective camera model, a linear pushbroom model and a full pushbroom model.

In order to make the results directly comparable, the same ground control points and image to image correspondences were used for camera model computations in all three experiments. (The number of tie or match points in computation of the pin-hole camera is an exception where 511 tie-points, instead of 100, were provided in an attempt to boost its accuracy.) In addition, the terrain model was also generated using the same set of match points.

The results of these three experiments are tabulated in Table 1. The first and the second row list the number of ground control points and the number of ties points used in the camera model computation. The third row gives the number of match points for which a point on the terrain was generated. The camera model accuracy, i.e., accuracy with which

	Pin-hole Model	Linear Push-broom Model	Full SPOT Model
Num. gc pts	25	25	25
Num. match pts	511	100	100
Num. terrain points	68,131	68,131	68,131
RMS error	11.13 pixels	0.80 pixels	0.73 pixels
Terrain accuracy	380.79m	35.67m	11.10m
Time	~5 sec.	~5 sec.	> 20 min.

Table 1: A comparison of the three camera models.

a ground point  $(x, y, z)^\top$  is mapped into its corresponding image point, listed in the fourth row. Finally, the RMS difference between the generated terrain and the ground truth (DMA DTED data) is given in the fifth row.

The attempt to model SPOT’s HRV cameras by perspective cameras yielded camera models with a combined accuracy of about 11 pixels. This is a large error because for a high platform such as a satellite, even a single pixel error can translate into a discrepancy of tens of meter along the horizontal and vertical dimensions (the exact amount depends on the pixel resolution and the look angles). This is reflected in the accuracy of the generated terrain which is as much as 380 meters off, on the average. Thus, as expected, a pin-hole camera is a poor approximation for pushbroom camera. The linear pushbroom, on the other hand, is quite competitive with the detailed model, both in terms of camera model accuracy, as well as the accuracy of the generated terrain.

The last entry on the fifth row (the 11.10m accuracy for the terrain generated by the complex model) is a little misleading since generated terrain is more accurate than the claimed accuracy of the ground-truth it is being compared with. This figure is a statement about the accuracy of the ground-truth, instead of the other way around. Figs. 4 and 5 show the terrain generated by the perspective and the full SPOT models, respectively. Fig. 5 can be regarded as the ground truth. In all these figures, the Pacific Ocean has been independently set to have an elevation of 0. Also, since the area covered is rather large (about  $60\text{km} \times 60\text{km}$ ), the terrain relief has been considerably exaggerated compared to the horizontal dimensions. We have not included the terrain generated by the linear pushbroom model because it is visually indistinguishable from that generated by the full model (Fig. 5).

Fig. 4 illustrates the distortion introduced when a partially perspective projection is modeled by a fully perspective camera. In order to better understand this distortion, the following experiment was conducted.

Using the full pushbroom model parameterized to an actual orbit and ephemeris data, and an artificial terrain model, a set of ground to image correspondences were computed, one such ground control point being computed every 120 pixels. This gave a  $51 \times 51$  grid of ground-control points covering approximately  $6000 \times 6000$  pixels. Next, these ground control points were used to instantiate the linear pushbroom model using the algorithm of section 3. In this

Figure 4: Terrain reconstructed from perspective model

Figure 5: Terrain reconstructed from full model

Figure 6: Error profile for linear pushbroom model

Figure 7: Error profile for perspective model

experiment, the locations of ground points were fixed for both the full and linear pushbroom models. The difference was measured between the corresponding image points as computed by each of the models. The absolute value of error as it varies across the image is shown in Fig. 6. The maximum error was less than 0.4 pixels with an RMS error of 0.16 pixels. As can be seen, for a complete SPOT image, the error incurred by using the linear pushbroom model is less than half a pixel, and much less over most of the image.

To test whether a perspective camera model could do as well, the same set of ground control points were modeled using a perspective camera model. The result was an RMS error of 16.8 pixels with a maximum pixel error of over 45 pixels. Figs 7. shows the error distribution across the image.