

On Reciprocity in Linear Time-Invariant Networks

by

B. D. O. Anderson and R. W. Newcomb

November 1965

Technical Report No. 6558-3

Prepared under

National Science Foundation Grant GK 237

SYSTEMS THEORY LABORATORY

STANFORD ELECTRONICS LABORATORIES

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ABSTRACT

A general time-domain definition of reciprocity is given in terms of network port variables, and this definition is applied to conclude the symmetry of network matrices, even in the case of active, nonfinite networks. A new proof is presented of the reciprocity of finite networks composed of time-invariant resistors, capacitors, inductors and transformers, and this proof is also applied to show the reciprocity of interconnections of a wide class of reciprocal networks.

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I. INTRODUCTION

We first consider a general definition of reciprocity for linear time-invariant networks and from this deduce certain equivalent definitions which depend on additional assumptions being made, such as the existence of an impedance matrix. The initial definition is a time-domain one; the property of reciprocity of a network is independent of whether or not the network inputs are Laplace-transformable, and to discuss reciprocity (as is often done) with inputs being restricted to being Laplace-transformable is therefore better avoided if possible.

The time-domain definition is initially in terms of voltage and current variables. An equivalent definition in terms of scattering variables (incident and reflected voltage waves) is given. This allows the examination of the effect the reciprocity constraint has on the scattering matrix when this latter exists. Here, as in the immittance matrix case, it is concluded that symmetry of the matrix is a consequence of reciprocity.

The third section of the paper considers primarily the case of networks composed of a finite number of positive-valued (passive) resistors, capacitors and inductors, together with multiport transformers. The scattering matrix (though not the impedance matrix) for such a network always exists [1], and the matrix is shown to be symmetric. The method used to prove this result is based on a representation of the network as a "cascade loading" [1], that is, the cascade connection of a network consisting entirely of opens and shorts, and a loading network that is a multiport of uncoupled resistors, capacitors, inductors, and transformers. Finally, it is shown that any interconnection of linear, passive, solvable, reciprocal time-invariant networks is again a reciprocal network.

II. RECIPROACITY FOR LINEAR TIME-INVARIANT NETWORKS

As explained in the introductory section, we are interested in defining reciprocity in the widest possible sense, that is, assuming linearity and time-invariance but as little else as possible. Definitions requiring for example that a unit impulse of current at port i gives a voltage at port j which is the same as the voltage at port i produced by a unit impulse of current at port j are unnecessarily restrictive. This particular definition requires the existence of an impedance matrix, and, as such, does not even apply to a network consisting of a network consisting of a simple transformer.

We offer what we believe to be the most general definition, posed in terms of earlier discussions of ways of defining networks [2], [3].

We assume that an n -port network \underline{N} permits voltage-current pairs $[\underline{v}, \underline{i}]$ (termed allowed pairs) at its terminals, where $\underline{v}, \underline{i}$ are real-valued n -vector functions of time, zero up until some finite time, and infinitely differentiable after this time. The physical reasoning behind these assumptions may be found in [2], [3]. We shall write $\underline{v} \in \mathcal{D}_+$ to signify that \underline{v} has these properties.

Suppose $[\underline{v}_1, \underline{i}_1]$ and $[\underline{v}_2, \underline{i}_2]$ are two arbitrary allowed pairs. Then by definition \underline{N} is reciprocal if for all such choices

$$\tilde{\underline{v}}_1 * \underline{i}_2 = \tilde{\underline{v}}_2 * \underline{i}_1 \quad (1)$$

The symbol $*$ denotes convolution; the superscript tilde \sim denotes matrix transposition.

If $\underline{v}_1 = [v_{1\alpha}]$, $\underline{i}_2 = [i_{2\alpha}]$ etc., (1) written in full becomes

$$\sum_{\alpha=1}^n \int_{-\infty}^{+\infty} v_{1\alpha}(t-\tau) i_{2\alpha}(\tau) d\tau = \sum_{\alpha=1}^n \int_{-\infty}^{+\infty} v_{2\alpha}(t-\tau) i_{1\alpha}(\tau) d\tau \quad (1')$$

Definition (1), which appears elsewhere [2], [4, p. 236], has been termed Lorentz reciprocity, as it is suggested by a theorem originally stated by Lorentz for electromagnetic systems. We comment further that since the various functions involved in (1) are zero up until some finite

time the convolutions are well defined, and the convolution product is commutative.

In preparation for dealing with networks possessing a scattering matrix, we introduce at this stage scattering variables $\underline{v}^i, \underline{v}^r$ (incident and reflected voltage vectors) for the network \underline{N} [5, p. 142]. These quantities are defined through

$$2\underline{v}^i = \underline{v} + \underline{i} \quad (2a)$$

$$2\underline{v}^r = \underline{v} - \underline{i} \quad (2b)$$

Note that by defining scattering variables we are not predicating the existence of a scattering matrix. Corresponding to allowed pairs $[\underline{v}_1, \underline{i}_1]$ and $[\underline{v}_2, \underline{i}_2]$ we have pairs $\left\{ \underline{v}_1^i, \underline{v}_1^r \right\}$ and $\left\{ \underline{v}_2^i, \underline{v}_2^r \right\}$, where the different brackets are to distinguish scattering variables from the ordinary variables.

Then we claim that an alternate statement of reciprocity is: \underline{N} is reciprocal if for arbitrary allowed $\left\{ \underline{v}_1^i, \underline{v}_1^r \right\}$ and $\left\{ \underline{v}_2^i, \underline{v}_2^r \right\}$

$$\underline{v}_1^i * \underline{v}_2^r = \underline{v}_2^i * \underline{v}_1^r \quad (3)$$

Equations (1) and (3) are strictly equivalent, so that (3) could equally well be taken as the reciprocity definition. To see for example that (3) implies (1), substitute for the variables \underline{v}_1^i etc. in (3) by using (2). On cancelling out like terms on each side of the resulting equation, (1) follows. In an equally simple fashion (3) follows from (1).

Let us now specialize \underline{N} so that it is linear, time-invariant and completely solvable, that is, \underline{N} possesses a (time-domain) scattering matrix [6]. The class of networks possessing scattering matrices is a more general one than the class possessing impedance matrices, [7, p. 122], for example, any finite linear time-invariant \underline{N} composed of standard passive-network elements which possesses an impedance matrix also possesses a scattering matrix, but not vice versa [1]. Accordingly we choose first to make this specialization, rather than assume the existence of an impedance matrix. The time-domain scattering matrix is used as this is a more fundamental matrix than the more common frequency domain matrix,

which exists if and only if the time-domain matrix is Laplace-transformable.

Since any physical network \underline{N} (active or passive) is nonanticipative, we shall assume that the scattering matrix $\underline{s} \equiv \underline{s}(t)$ is zero for $t < 0$, and maps incident voltages into reflected voltages through

$$\underline{v}^r = \underline{s} * \underline{v}^i \quad (4)$$

where $\underline{v}^i \in \underline{\mathcal{D}}_+$ but is otherwise arbitrary. If all quantities are Laplace-transformable, then (4) implies the more familiar equation $V^r(p) = S(p)V^i(p)$.

In general \underline{s} will not be a function; it is however shown in [6] that \underline{s} will be a distribution in the variable t [8], typically involving a delta function and a unit step function. Because \underline{s} is identically zero for negative values of the argument, \underline{s} is said to be in the space $\underline{\mathcal{D}}'_+$ [9, p. 28] of distributions with support bounded on the left. The variables \underline{v}^r and \underline{v}^i being in the space $\underline{\mathcal{D}}_+$ are also in the space $\underline{\mathcal{D}}'_+$.

Substituting from (4) into (3) we have

$$\tilde{\underline{v}}_1^i * (\underline{s} * \underline{v}_2^i) = \tilde{\underline{v}}_2^i * (\underline{s} * \underline{v}_1^i) \quad (5a)$$

A theorem of L. Schwartz [9, p. 28] shows that the convolution products in this equation are associative and commutative since the various factors are all in the space $\underline{\mathcal{D}}'_+$. Accordingly

$$\begin{aligned} \tilde{\underline{v}}_1^i * \underline{s} * \underline{v}_2^i &= \tilde{\underline{v}}_2^i * \underline{s} * \underline{v}_1^i \\ &= \tilde{\underline{v}}_1^i * \tilde{\underline{s}} * \underline{v}_2^i \end{aligned} \quad (5b)$$

We may choose \underline{v}_1^i and \underline{v}_2^i arbitrarily; take in particular \underline{v}_1^i to have all entries zero except the k -th, and \underline{v}_2^i to have all entries zero except the l -th. The nonzero entries of \underline{v}_1^i and \underline{v}_2^i are arbitrary $\underline{\mathcal{D}}_+$ functions. Then

$$v_{1k}^i * s_{kl} * v_{2l}^i = v_{1k}^i * s_{lk} * v_{2l}^i \quad (6)$$

which implies that

$$s_{kl} = s_{lk} \quad (7)$$

Observe also that (7) implies (5a). This yields the following theorem.
Theorem 1. A linear time-invariant completely solvable network \underline{N} is reciprocal if and only if its (time-domain) scattering matrix is symmetric.

In the case where the Laplace transform $\mathcal{L}[\underline{s}(t)] = S(p)$ exists we have

Corollary. A linear time-invariant solvable network \underline{N} possessing a scattering matrix $S(p)$ is reciprocal if and only if $S(p)$ is symmetric.

We comment that the preceding proof does not assume the existence $\mathcal{L}[\underline{s}]$, $\mathcal{L}[\underline{v}^i]$, $\mathcal{L}[\underline{v}^r]$, and is accordingly more general than any proof considering all quantities to be defined in the (complex) frequency domain. It should also be noted that the result is independent of the passivity (or lack of it) of the network \underline{N} . Neither does \underline{N} have to be finite.

What now of the linear time-invariant network which possesses an impedance matrix $\underline{z}(t)$, with possibly $Z(p)$ existing as well? Arguments similar to those used to establish Theorem 1, but starting from (1) rather than (3) yield:

Theorem 2. A linear time-invariant network \underline{N} possessing an impedance matrix $\underline{z}(t)$ (and perhaps $Z(p)$) is reciprocal if and only if $\underline{z}(t)$ (and $Z(p)$) is symmetric.

A similar theorem holds of course for admittance matrices.

Note that if $S(p)$ and $Z(p)$ both exist, then the symmetry of one follows immediately from the symmetry of the other through the equations [10, p. 242]

$$S(p) = [Z(p) + 1]^{-1}[Z(p) - 1] \quad (8a)$$

$$Z(p) = [1 - S(p)]^{-1}[1 + S(p)] \quad (8b)$$

III. RECIPROCIITY FOR FINITE PASSIVE LINEAR TIME-INVARIANT NETWORKS AND INTERCONNECTIONS OF RECIPROCAL NETWORKS

In this section we consider networks composed of a finite number of positive resistors, capacitors, inductors, and multiport transformers, that is, the most general kind of linear passive finite time-invariant network composed of reciprocal elements. The reciprocity of such a network was established by McMillan [4], and more recently for example by de Buda [11]. We present here a simple proof relying on the result established elsewhere [1] that the scattering matrix of such a network exists in the complex frequency domain (p domain), and further apply this result to the interconnections of passive reciprocal networks.

It is clear, and shown in [1], that any finite linear time-invariant n -port network \underline{N} composed of positive resistors, capacitors and inductors, together with multiport transformers, can be represented as the cascade connection of a network \underline{N}_Σ composed entirely of opens and shorts, terminated in a network \underline{N}_ρ consisting of all the resistors, capacitors, etc., of \underline{N} unconnected to each other. This is shown in Fig. 1.

A multiport transformer may be described by the equations

$$\underline{v}_1 = \tilde{T}\underline{v}_2 \quad (9a)$$

$$\underline{i}_2 = -T\underline{i}_1 \quad (9b)$$

where T is a constant $m \times n$ matrix, the transformer having n primary and m secondary ports. The vectors $\underline{v}_1, \underline{v}_2$ are the primary and secondary voltages, and $\underline{i}_1, \underline{i}_2$ the primary and secondary currents. The transformer has the scattering matrix

$$S(p) = \begin{bmatrix} (1_n + \tilde{T}T)^{-1}(\tilde{T}T - 1_n) & 2(1_n + \tilde{T}T)^{-1}\tilde{T} \\ 2T(1_n + \tilde{T}T)^{-1} & (1_m + T\tilde{T})^{-1}(1_m - T\tilde{T}) \end{bmatrix} \quad (10)$$

which is easily verified to be symmetric. As a consequence, \underline{N}_Σ has a symmetric scattering matrix Σ and is therefore reciprocal, since, as is shown in [1], \underline{N}_Σ is subject to the same constraining relations as

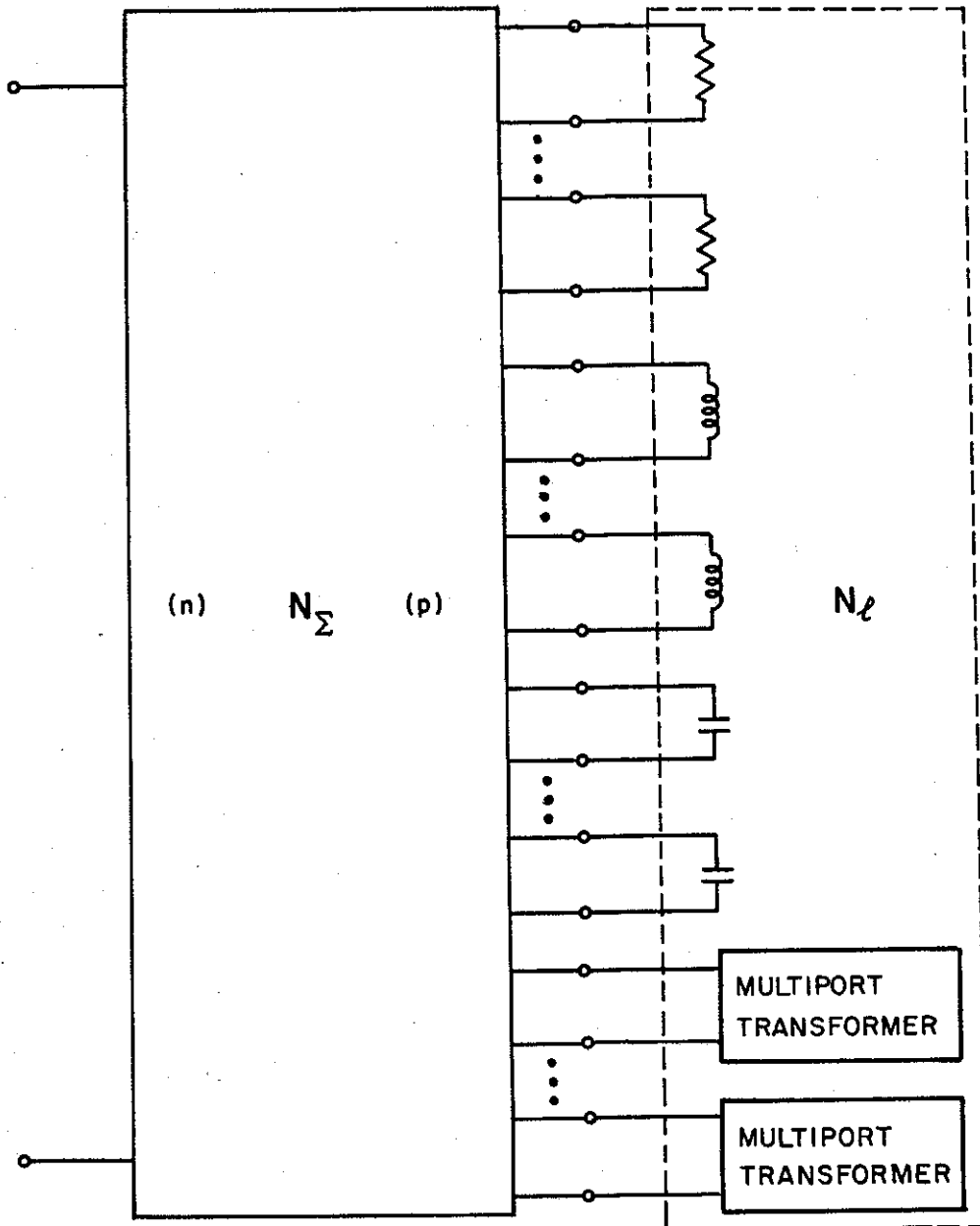


Fig. 1: Cascade Loading Representation of N

a multiport transformer. The network \underline{N}_ℓ also has a symmetric scattering matrix S_ℓ , this being the (matrix) direct sum of a number of symmetric matrices (corresponding to each of the network elements of \underline{N} , each of which is reciprocal).

We partition Σ as

$$\Sigma = \begin{bmatrix} \Sigma_{11} & \Sigma_{12} \\ \Sigma_{21} & \Sigma_{22} \end{bmatrix} = \tilde{\Sigma}$$

where Σ_{11} is $n \times n$, corresponding to the input ports of \underline{N} , Σ_{22} is $p \times p$, where \underline{N}_ℓ has p ports.

The scattering matrix S of the cascade loading interconnection may be evaluated using methods outlined in [12] as

$$S = \Sigma_{11} + \Sigma_{12} S_\ell (I_p - \Sigma_{22} S_\ell)^{-1} \Sigma_{21} \quad (11a)$$

or equivalently

$$S = \Sigma_{11} + \Sigma_{12} (I_p - S_\ell \Sigma_{22})^{-1} S_\ell \Sigma_{21} \quad (11b)$$

Difficulties arise due to the question of the existence of the inverse of $I_p - \Sigma_{22} S_\ell$ (or $I_p - S_\ell \Sigma_{22}$) and are dealt with in the appendix. Here we shall simply assume the inverses exist. Taking the transpose of (11a):

$$\tilde{S} = \tilde{\Sigma}_{11} + \tilde{\Sigma}_{21} (I_p - \tilde{S}_\ell \tilde{\Sigma}_{22})^{-1} \tilde{S}_\ell \tilde{\Sigma}_{12}$$

Using the symmetry of Σ and S_ℓ ,

$$\tilde{S} = \Sigma_{11} + \Sigma_{12} (I_p - S_\ell \Sigma_{22})^{-1} S_\ell \Sigma_{21}$$

Using (11b) it follows that

$$S = \tilde{S} \quad (12)$$

By the corollary to Theorem 1, this implies that the network \underline{N} is

reciprocal. Hence we have the following statement.

Theorem 3. A network consisting of a finite number of passive time-invariant resistors, capacitors, inductors and multiport transformers, is reciprocal, and in fact possesses a symmetric scattering matrix.

This result is capable of almost immediate generalization. Suppose \underline{N}_1 and \underline{N}_2 are any two linear, passive, time-invariant reciprocal networks possessing scattering matrices $S_1(p)$ and $S_2(p)$ and that \underline{N}_1 and \underline{N}_2 are connected together in some arbitrary fashion. As before, we represent the interconnecting network as \underline{N}_Σ with scattering matrix Σ , and the load network as \underline{N}_ℓ , consisting of \underline{N}_1 and \underline{N}_2 uncoupled. See Fig. 2. The network \underline{N}_ℓ is of course linear, passive, time-invariant and reciprocal, and possesses a scattering matrix equal to the direct sum of $S_1(p)$ and $S_2(p)$. The arguments used to establish Theorem 3 depend merely on the passivity and symmetry of the matrices involved rather than, for example, the fact that these matrices are derived from finite networks, and accordingly they carry through to show:

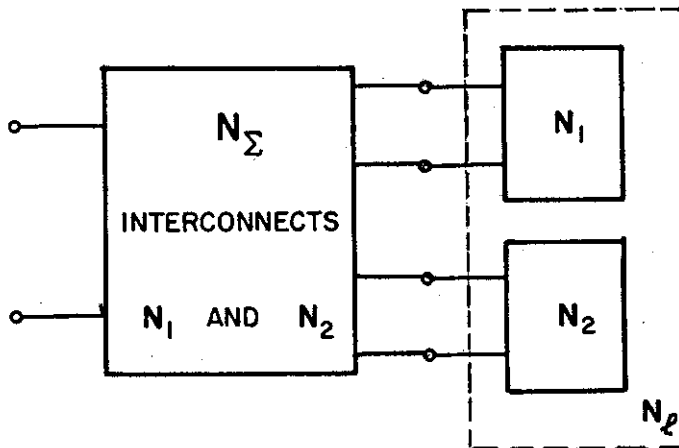


Fig. 2: General Interconnection of Two Reciprocal Networks

Theorem 4. Let \underline{N}_1 and \underline{N}_2 be two linear, passive, time-invariant reciprocal networks possessing scattering matrices $S_1(p)$ and $S_2(p)$. Then any arbitrary interconnection of \underline{N}_1 and \underline{N}_2 is also reciprocal, and in fact possesses a symmetric scattering matrix $S(p)$.

IV. CONCLUSIONS

Reciprocity is a meaningful concept for linear time-invariant networks; existence of impedance matrices or Laplace-transformable inputs are not necessary prerequisites for a discussion of reciprocity. A time-domain definition of reciprocity which encompasses the more common but less general definitions usually given is considered, and an equivalent statement in terms of the often more useful scattering variables is given. The symmetry of network matrices when they exist is implied by reciprocity, and this property is independent of properties such as network passivity. A new proof is given of the reciprocity of finite passive resistor, capacitor, inductor, transformer networks which is an application of earlier work [1]. This proof is independent of the existence of chain or impedance matrices.

ACKNOWLEDGEMENT

The authors wish to acknowledge the National Science Foundation under Grants NSF GP-520 and NSF GK-237 for the support of the research of this report. The first author would also like to acknowledge the financial support of the Services Canteens Trust Fund, an agency of the Australian Government, and the United States Educational Foundation in Australia for a Fulbright Travelling Grant. The expert assistance of Barbara Serrano in typing the manuscript is also gratefully acknowledged.

APPENDIX

Suppose $(1_p - \Sigma_{22} S_\ell)^{-1}$ does not exist. Now, as is pointed out in [1], $\begin{bmatrix} \Sigma_{11} & \Sigma_{12} S_\ell \\ \Sigma_{21} & \Sigma_{22} S_\ell \end{bmatrix}$ and $\Sigma_{22} S_\ell$ are passive scattering matrices, and

accordingly [7, p. 121], there exists a constant orthogonal matrix T such that

$$\begin{bmatrix} 1 & 0 \\ 0 & \tilde{T} \end{bmatrix} \begin{bmatrix} \Sigma_{11} & \Sigma_{12} S_\ell \\ \Sigma_{21} & \Sigma_{22} S_\ell \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & T \end{bmatrix} = \begin{bmatrix} \Sigma_{11} & \hat{\Sigma}_{12} & 0 \\ \hat{\Sigma}_{21} & \hat{\Sigma}_{22} & 0 \\ 0 & 0 & 1_r \end{bmatrix}$$

with $\tilde{T} \Sigma_{21} = \begin{bmatrix} \hat{\Sigma}_{21} \\ 0 \end{bmatrix}$, $\Sigma_{12} S_\ell T = \begin{bmatrix} \hat{\Sigma}_{12} & 0 \end{bmatrix}$ and $\det(1_{p-r} - \hat{\Sigma}_{22}) \neq 0$,

that is $(1_{p-r} - \hat{\Sigma}_{22})^{-1}$ exists. Range space arguments following those given in [1] then show that in place of

$$S = \Sigma_{11} + \Sigma_{12} S_\ell (1_p - \Sigma_{22} S_\ell)^{-1} \Sigma_{21} \quad (11a)$$

or equivalently

$$\begin{aligned} S &= \Sigma_{11} + \Sigma_{12} S_\ell T \left\{ \tilde{T} (1_p - \Sigma_{22} S_\ell) T \right\}^{-1} \tilde{T} \Sigma_{21} \\ &= \Sigma_{11} + \begin{bmatrix} \hat{\Sigma}_{12} & 0 \end{bmatrix} \begin{bmatrix} (1_{p-r} - \hat{\Sigma}_{22}) & 0 \\ 0 & 0 \end{bmatrix}^{-1} \begin{bmatrix} \hat{\Sigma}_{21} \\ 0 \end{bmatrix} \end{aligned}$$

we have

$$S = \Sigma_{11} + \hat{\Sigma}_{12} (1_{p-r} - \hat{\Sigma}_{22})^{-1} \hat{\Sigma}_{21} \quad (13a)$$

In place of

$$S = \Sigma_{11} + \Sigma_{12} (I_p - S_{\ell} \Sigma_{22})^{-1} S_{\ell} \Sigma_{21} \quad (11b)$$

or equivalently

$$\begin{aligned} S &= \Sigma_{11} + \tilde{\Sigma}_{21} \overbrace{(I_p - \Sigma_{22} S_{\ell})}^{-1} \tilde{S}_{\ell} \tilde{\Sigma}_{12} \\ &= \Sigma_{11} + \tilde{\Sigma}_{21} \mathbb{T} \overbrace{\mathbb{T} (I_p - \Sigma_{22} S_{\ell}) \mathbb{T}}^{-1} \tilde{\mathbb{T}} \tilde{S}_{\ell} \tilde{\Sigma}_{12} \\ &= \Sigma_{11} + \begin{bmatrix} \tilde{\Sigma}_{21} & 0 \end{bmatrix} \begin{bmatrix} \overbrace{(I_{p-r} - \tilde{\Sigma}_{22})}^{-1} & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \tilde{\Sigma}_{12} \\ 0 \end{bmatrix} \end{aligned}$$

we have

$$S = \Sigma_{11} + \tilde{\Sigma}_{21} \overbrace{(I_{p-r} - \tilde{\Sigma}_{22})}^{-1} \tilde{\Sigma}_{12} \quad (13b)$$

From (13a) and (13b) we conclude that

$$S = \tilde{S} \quad (12)$$

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