



**IFAC**

International Federation of Automatic Control

**BENCHMARK PROBLEMS FOR  
CONTROL SYSTEM DESIGN**

**REPORT OF THE IFAC THEORY COMMITTEE**

**Edited by Edward J. Davison, Chairman**

**May 1990**

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**Problem #90-08 LOWER ORDER CONTROLLER DESIGN FOR A HIGH ORDER PLANT**

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**(A) Motivation for the Problem**

The motivation for the problem is to provide a uniform testbed for the evaluation of different approaches and algorithms in design of low-order linear feedback controllers for a high-order plant (typical of most industrial problems). In this case, a design example from the aircraft industry is provided. The open-loop plant model possesses key features that render the application of conventional design techniques difficult, if not impossible, in achieving the specified design requirements. They are:

- (i) High dynamic order (35<sup>th</sup>-order);
- (ii) Multivariable system with two inputs and two outputs;
- (iii) Open-loop instability (i.e., Flutter mode);
- (iv) Numerous highly oscillatory modes (i.e., lightly damped structural modes);
- (v) Nonminimum-phase characteristics.

**(B) Brief Description of Problem Origin**

This plant is an aeroelastic model for a modified Boeing B-767 airplane, at a flutter condition, that was used in a research study of active control technology [1] where a linear-quadratic-gaussian (LQG)-based design has been developed for flutter control and gust load alleviation. The resulting 55<sup>th</sup>-order controller has been subsequently reduced to a 10<sup>th</sup>-order controller for practical implementation using a standard modal residualization technique. Description of the design philosophy and related details on final design performance can be found in reference [1] and [2]. Additional results on controller reduction applied to this problem can be found in reference [3].

**(C) Problem Description**

The problem is to synthesize a linear feedback control-law of low order (preferably less than 10) that achieves the following design objectives:

- (i) Stabilizes the flutter mode with damping of at least 0.015;
- (ii) Provides minimal damping of 0.1 to the remaining low-frequency modes;
- (iii) Reduces the mean-square responses of aircraft dynamic load variables to turbulence;

(iv) Possesses desirable robustness in terms of phase and gain margins at each control loop.

The following are a set of design requirements for the benchmark problem:

- (i) Minimum damping of 0.015 for the flutter mode identified by its frequency near  $\omega \approx 20$  rad/sec (e.g., flutter mode damping achieved by the LQG controller in references [1] and [2] is 0.074);
- (ii) Minimum damping of 0.40 for the remaining low-frequency modes (e.g., aircraft short-period mode, compensator modes, etc.);
- (iii) Adequate attenuation of aircraft dynamic load responses to a 10ft/sec rms turbulence  $w_1$  (e.g., comparable with those achieved by the LQG controller in references [1] and [2]);
- (iv) Moderate control activities based on mean-square responses of control deflections and their rates to a 10ft/sec turbulence  $w_1(t)$  (i.e., comparable with results in references [1] and [2]);
- (v) Adequate phase and gain margins:
  - Gain margin of  $\pm 6$  dB
  - Phase margin of  $\pm 45^\circ$

in the elevator and aileron control loops. Stability margins are evaluated one-loop-at-a-time using classical single-loop analysis).

The linear feedback control system could be designed directly, or from the reduction of a high-order controller (for example, using a previously designed LQG controller of references [1] and [2] meets the above design objectives). The LQG controller design in references [1] and [2] was obtained from the following quadratic cost function with process and sensor noise characteristics for the plant model described in Appendix I.

• Design cost function: The cost function is of the form:

$$J = \int_0^{\infty} [Q_1 y_1^2(t) + Q_2 y_2^2(t) + Q_3 y_3^2(t) + R_1 u_1^2(t) + R_2 u_2^2(t)] dt$$

The following output variables  $y_i$  ( $i = 1, 2, 3$ ) have been penalized in the cost function with weighting factors  $Q_i$  ( $i = 1, 2, 3$ ):

Output Variables $y_i$	Weighting Factor $Q_i$
(1) Inboard bending moment (BMOMI)	$3.76 \times 10^{-14}$
(2) Inboard torsion (TORI)	$1.20 \times 10^{-13}$
(3) Outboard torsion (TORO)	$2.45 \times 10^{-12}$

along with the input variables  $u_i$  and their weighting factors  $R_i$  ( $i = 1, 2$ ):

Input Variable $u_i$	Weighting Factor $R_i$
(1) Elevator control (ELEV)C)	$3.647 \times 10^2$
(2) Aileron control (AILC)	$1.459 \times 10^1$

- **Process and sensor noise characteristics:** A Kalman filter was designed using the measurement of aircraft pitch rate QCG and wing-tip acceleration WTIPDD. The process noises  $w_i$  ( $i = 1, 2, 3$ ) have input distribution matrix  $B_n$  and spectral densities  $W_i$  ( $i = 1, 2, 3$ ):

Process Noise $w_i$	Spectral Density $W_i$
(1) Vertical gust (WG)	$2.8224 \times 10^4$ (in/sec) <sup>2</sup> /rad/sec
(2) Elevator input noise (ELEV)N)	$2.742 \times 10^{-2}$ (rad) <sup>2</sup> /(rad/sec)
(3) Aileron input noise (AILN)	$6.854 \times 10^{-4}$ (rad) <sup>2</sup> /(rad/sec)

The sensor noises  $v_i$  ( $i = 1, 2$ ) for the above two measurements have the following spectral densities:

Sensor Noise $v_i$	Spectral Density $V_i$
(1) Pitch rate (QCG)	$6.85 \times 10^{-6}$ (rad) <sup>2</sup> /(rad/sec)
(2) Wing-tip acceleration (WTIPDD)	$3.73 \times 10^2$ (in/sec <sup>2</sup> ) <sup>2</sup> /(rad/sec)

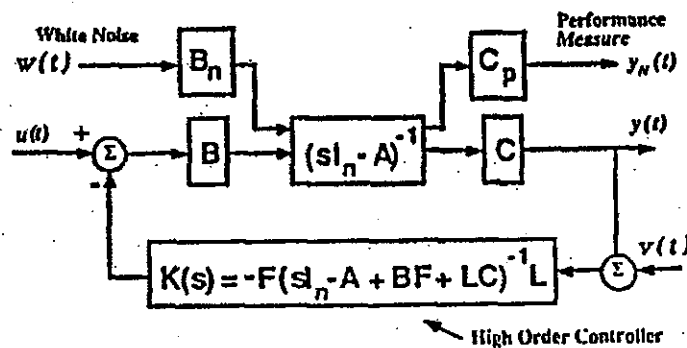


Fig.1 Closed-loop system structure with a full order controller

Appendix I shows the resulting gain matrices  $F$  and  $L$  of the regulator and Kalman filter design respectively, using the above design parameters. Figure 1 shows a block diagram of the closed-loop system constructed with a full-order LQG controller where the matrices  $A$ ,  $B$ ,  $C$ ,  $B_n$ ,  $C_p$ ,  $F$  and  $L$  are given in Appendix I.

For convenience, design evaluation of the above full-order LQG controller, a 10<sup>th</sup>-order (reduced) controller [1,2] and a 5<sup>th</sup>-order controller [3] are given in Table 1.

**Table 1**  
Closed-Loop Evaluation for Full (LQG Design) and Reduced Order Controllers

Controller Order	55 <sup>th</sup> [2]	10 <sup>th</sup> [2]	5 <sup>th</sup> [3,LCFV]
Flutter Mode Damping	0.074	0.070	0.0501
<b>Inboard Wing Station:<sup>†</sup></b>			
Bending Moment ( $\times 10^5$ in-lbs)	2.348	2.349	2.624
Shear (lbs)	854.	861.	950.
Torsion ( $\times 10^4$ in-lbs)	4.437	4.597	4.969
<b>Outboard Wing Station:<sup>†</sup></b>			
Bending Moment ( $\times 10^5$ in-lbs)	0.259	0.262	0.239
Shear (lbs)	259.	260.	286.
Torsion ( $\times 10^4$ in-lbs)	1.196	1.206	1.274
<b>Control Surface Activities:<sup>†</sup></b>			
Elevator Control Deflection (rad)	0.00054	0.00056	0.000339
Elevator Control Surface Rate (rad/sec)	0.00407	0.00436	0.00401
Aileron Control Deflection (rad)	0.00158	0.00163	0.00176
Aileron Control Surface Rate (rad/sec)	0.0275	0.0276	0.0332
<b>Stability Margins:<sup>*</sup></b>			
Elevator Control Loop: Gain Margin (dB)	15.9	36.4	18.2
Phase Margin (deg)	180	180	-102
Aileron Control Loop: Gain Margin (dB)	14	25	(-15,14.1)
Phase Margin (deg)	58.6	(-138.9,146)	(-140,82.3)

<sup>†</sup> Root-Mean-Square (rms) to a 10ft/sec vertical Dryden turbulence [by injecting white-noise at the input  $w_1(t)$  with a power spectral density of  $(10ft/sec)^2(rad/sec)$ ].

<sup>\*</sup> Frequency range considered is  $0.01 \leq \omega \leq 100$  rad/sec.

#### (D) Previous Results Obtained

Discussion of the aircraft aeroelastic model and design in the LQG Controller can be found in the following references:

1. Ly, U.-L. and D. Gangsaas, "Application of Modified Linear Quadratic Gaussian Design to Active Control of a Transport Airplane", *AIAA, Guidance and Control Conference*, Boulder, Colorado, August 1979.
2. Ly, U.-L., D. Gangsaas and D.C. Norman, "Practical Gust Load Alleviation and Flutter Suppression Control Laws Based on an LQG Methodology", *AIAA, Aerospace Sciences Meeting*, 1981.

A discussion of some controller reduction methods used on the full order LQG designed controller to generate lower order controllers appears in the following:

3. Liu, Y., B.D.O. Anderson, U.-L. Ly, "Coprime Factorization Controller Reduction with Bezout Identity Induced Frequency Weighting", *Automatica*, to appear.

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**Appendix I**  
**Plant Model State Matrices**

Aeroelastic model of a modified B767-aircraft at a flutter condition is a linear state model of the form

$$\dot{x}(t) = Ax(t) + Bu(t) + B_n w(t)$$

where

- $x(t)$  is a state vector (of dimension 55) containing the aircraft rigid and aeroelastic modes, actuator modes, Dryden turbulence filter and other noise shaping filters;
- $u(t)$  is a control vector (of dimension 2) containing the elevator control ELEV and the aileron control AILC;
- $w(t)$  is a process noise input vector (of dimension 3) containing the vertical turbulence input  $w_1(t)$ , the elevator noise input  $w_2(t)$  and the aileron noise input  $w_3(t)$ .

The sensor output  $y(t) = [QCG \quad WTIPDD]^T$  consists of the aircraft pitch rate QCG and the wing-tip acceleration WTIPDD variables and is given by

$$y(t) = Cz(t) + v(t)$$

The performance output variables

$$y_N(t) = [SHRI, BMOMI, TORI, SHRO, BMOMO, TORO, ELD, EL, ALOD, AILO]^T$$

given by

$$y_N(t) = C_p x(t)$$

represent those outputs to be used in the covariance analysis of the aircraft subjected to a vertical turbulence of 10ft/sec rms. They represent the dynamic loads of the aircraft at the inboard and outboard wing stations, the elevator and aileron control deflections and rates respectively, i.e.,

SHRI:	Shear force at the inboard wing station (lbs)
BMOMI:	Bending moment at the inboard wing station (in-lbs)
TORI:	Torsion at the inboard wing station (in-lbs)
SHRO:	Shear force at the outboard wing station (lbs)
BMOMO:	Bending moment at the outboard wing station (lbs)
TORO:	Torsion at the outboard wing station (in-lbs)
ELD:	Elevator control surface rate (rad/sec)
EL:	Elevator control surface deflection (rad)
ALOD:	Aileron control surface rate (rad/sec)
AILO:	Aileron control surface deflection (rad)

A closed-loop system with a full-order LQG controller is shown in Figure 1. State matrices  $A$ ,  $B$ ,  $B_n$ ,  $C$  and  $C_p$  along with the full-state feedback gain matrix  $F$  and the Kalman gain matrix  $L$  corresponding to the LQG controller in [1,2] are shown below.







X15	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-2561.	13.14	-0.2426	-1080.	48.49
X16	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	6593.	-19.32	0.3841	-3983.	-12.93
X17	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-2212.	-12.28	0.1229	-1647.	-15.130
X18	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	6321.	-27.17	0.2049	-1045.	-15.59
X19	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.3964E+04	-17.24	3.5851E-02	562.0	-25.48
X20	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2322.	-20.08	0.3605	902.6	-1.623
X21	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-303.7	2.624	-0.1208	1129.	4.399
X22	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	542.8	0.5789	0.1194	-1258.	-6.993
X23	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-527.1	-36.01	0.3072	-1267.	7.583
X24	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2658.	3.812	-3.7101E-02	-49.11	-4.347
X25	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	2.5341E+04	-36.45	0.4514	4360.	-131.3
X26	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	6538.	-28.56	0.3244	3790.	90.71
X27	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	4.2048E+04	-59.43	0.7558	2501.	-17.39
X28	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	210.6	-39.51	0.5076	-470.4	-18.75
X29	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
X30	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	994.2	13.57	-2.1971E-02	828.4	12.90
X31	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	769.2	10.60	-9.2043E-02	810.0	19.07
X32	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	4.2702E+04	-120.7	1.940	-3077.	35.90
X33	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-7.6982E+04	140.6	-2.796	-348.3	-38.56
X34	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-288.8	-0.9428	2.3831E-02	-1499.	0.9758
X35	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-2237.	8.455	-0.1565	-6578.	49.50
X36	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-1.6942E+04	94.43	-1.144	-60.89	0.2221
X37	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-1.2513E+04	68.02	-0.6821	-29.37	0.4639
X38	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	5748.	-35.78	0.2067	-39.31	-0.6830
X39	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-1.4657E+04	216.8	-0.6615	123.4	9.043
X40	-109.3	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-4089.	-258.1	-1.059	33.03	-2.040
X41	-11.72	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	7940.	309.0	1.175	61.04	2.311
X42	0.0000E+00	-11.79	-304.6	0.0000E+00	0.0000E+00	9582.	37.30	-3.1126E-02	140.9	2.627
X43	0.0000E+00	304.6	-11.79	0.0000E+00	0.0000E+00	9474.	41.40	-5.0827E-02	156.3	3.098
X44	0.0000E+00	0.0000E+00	0.0000E+00	-33.27	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
X45	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-221.2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELEV	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.000	0.0000E+00	0.0000E+00	0.0000E+00
ELEV0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELEV00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-8.0000E+05	-6.0800E+04	-1060.	0.0000E+00	0.0000E+00
AIL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.000
AILD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILDD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
WIND1	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-8.0000E+05	-6.0800E+04
WIND2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ENOISE	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ANOISE	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

	AILDD	WIND1	WIND2	ENOISE	ANOISE
X1	-0.1517	0.0000E+00	-3.159	0.0000E+00	0.0000E+00
X2	-5.0292E-02	0.0000E+00	1.779	0.0000E+00	0.0000E+00
X3	-7.4279E-06	0.0000E+00	5.3132E-03	0.0000E+00	0.0000E+00
X4	-1.1816E-05	0.0000E+00	8.0111E-03	0.0000E+00	0.0000E+00
X5	1.2317E-03	0.0000E+00	0.1066	0.0000E+00	0.0000E+00
X6	-3.9645E-03	0.0000E+00	-0.4078	0.0000E+00	0.0000E+00
X7	1.1391E-02	0.0000E+00	0.1001	0.0000E+00	0.0000E+00
X8	-2.8823E-03	0.0000E+00	-0.1571	0.0000E+00	0.0000E+00
X9	-4.9071E-02	0.0000E+00	-1.060	0.0000E+00	0.0000E+00
X10	-4.5192E-02	0.0000E+00	0.4854	0.0000E+00	0.0000E+00
X11	1.0263E-03	0.0000E+00	-2.733	0.0000E+00	0.0000E+00
X12	1.1647E-02	0.0000E+00	2.067	0.0000E+00	0.0000E+00
X13	-0.1277	0.0000E+00	3.001	0.0000E+00	0.0000E+00
X14	0.2540	0.0000E+00	3.544	0.0000E+00	0.0000E+00
X15	-0.3712	0.0000E+00	-7.199	0.0000E+00	0.0000E+00
X16	1.0825E-02	0.0000E+00	7.207	0.0000E+00	0.0000E+00
X17	2.0187E-02	0.0000E+00	0.6186	0.0000E+00	0.0000E+00
X18	6.4588E-02	0.0000E+00	1.076	0.0000E+00	0.0000E+00
X19	0.1072	0.0000E+00	2.821	0.0000E+00	0.0000E+00
X20	7.7575E-02	0.0000E+00	-0.7866	0.0000E+00	0.0000E+00
X21	-2.7240E-02	0.0000E+00	-0.1111	0.0000E+00	0.0000E+00
X22	2.9297E-02	0.0000E+00	1.509	0.0000E+00	0.0000E+00
X23	-6.5626E-03	0.0000E+00	-0.3659	0.0000E+00	0.0000E+00
X24	-8.4969E-03	0.0000E+00	0.8635	0.0000E+00	0.0000E+00
X25	0.8394	0.0000E+00	7.433	0.0000E+00	0.0000E+00
X26	-0.3495	0.0000E+00	-15.36	0.0000E+00	0.0000E+00
X27	0.1113	0.0000E+00	4.570	0.0000E+00	0.0000E+00
X28	0.1395	0.0000E+00	-0.2771	0.0000E+00	0.0000E+00
X29	0.0000E+00	0.0000E+00	-1.251	0.0000E+00	0.0000E+00
X30	-3.6967E-02	0.0000E+00	-0.5031	0.0000E+00	0.0000E+00
X31	-8.1012E-02	0.0000E+00	-0.4524	0.0000E+00	0.0000E+00
X32	-0.2467	0.0000E+00	-1.592	0.0000E+00	0.0000E+00
X33	0.1981	0.0000E+00	1.956	0.0000E+00	0.0000E+00
X34	-4.1943E-02	0.0000E+00	-5.981	0.0000E+00	0.0000E+00
X35	-0.4980	0.0000E+00	-10.88	0.0000E+00	0.0000E+00
X36	-1.1955E-02	0.0000E+00	-1.121	0.0000E+00	0.0000E+00
X37	-9.9611E-03	0.0000E+00	0.1532	0.0000E+00	0.0000E+00
X38	7.8189E-03	0.0000E+00	-0.4254	0.0000E+00	0.0000E+00
X39	-8.7434E-02	0.0000E+00	-0.7886	0.0000E+00	0.0000E+00
X40	2.3536E-02	0.0000E+00	-0.1053	0.0000E+00	0.0000E+00

X41	-2.8729E-02	0.0000E+00	-2.007	0.0000E+00	0.0000E+00
X42	-1.8542E-02	0.0000E+00	0.1886	0.0000E+00	0.0000E+00
X43	-2.2171E-02	0.0000E+00	9.2049E-03	0.0000E+00	0.0000E+00
X44	0.0000E+00	0.0000E+00	-17.07	0.0000E+00	0.0000E+00
X45	0.0000E+00	0.0000E+00	-37.83	0.0000E+00	0.0000E+00
ELEV	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELEVDD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELEVDD	0.0000E+00	0.0000E+00	0.0000E+00	-1.6000E+07	0.0000E+00
AIL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILD	1.000	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILDD	-1060.	0.0000E+00	0.0000E+00	0.0000E+00	-1.6000E+07
WIND1	0.0000E+00	0.0000E+00	-0.2668	0.0000E+00	0.0000E+00
WIND2	0.0000E+00	1.000	-1.833	0.0000E+00	0.0000E+00
ENOISE	0.0000E+00	0.0000E+00	0.0000E+00	-20.00	0.0000E+00
ANOISE	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	-20.00

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	ELEV	AILC
X1	0.0000E+00	0.0000E+00
X2	0.0000E+00	0.0000E+00
X3	0.0000E+00	0.0000E+00
X4	0.0000E+00	0.0000E+00
X5	0.0000E+00	0.0000E+00
X6	0.0000E+00	0.0000E+00
X7	0.0000E+00	0.0000E+00
X8	0.0000E+00	0.0000E+00
X9	0.0000E+00	0.0000E+00
X10	0.0000E+00	0.0000E+00
X11	0.0000E+00	0.0000E+00
X12	0.0000E+00	0.0000E+00
X13	0.0000E+00	0.0000E+00
X14	0.0000E+00	0.0000E+00
X15	0.0000E+00	0.0000E+00
X16	0.0000E+00	0.0000E+00
X17	0.0000E+00	0.0000E+00
X18	0.0000E+00	0.0000E+00
X19	0.0000E+00	0.0000E+00
X20	0.0000E+00	0.0000E+00
X21	0.0000E+00	0.0000E+00
X22	0.0000E+00	0.0000E+00
X23	0.0000E+00	0.0000E+00
X24	0.0000E+00	0.0000E+00
X25	0.0000E+00	0.0000E+00
X26	0.0000E+00	0.0000E+00
X27	0.0000E+00	0.0000E+00
X28	0.0000E+00	0.0000E+00
X29	0.0000E+00	0.0000E+00
X30	0.0000E+00	0.0000E+00
X31	0.0000E+00	0.0000E+00
X32	0.0000E+00	0.0000E+00
X33	0.0000E+00	0.0000E+00
X34	0.0000E+00	0.0000E+00
X35	0.0000E+00	0.0000E+00
X36	0.0000E+00	0.0000E+00
X37	0.0000E+00	0.0000E+00
X38	0.0000E+00	0.0000E+00
X39	0.0000E+00	0.0000E+00
X40	0.0000E+00	0.0000E+00
X41	0.0000E+00	0.0000E+00
X42	0.0000E+00	0.0000E+00
X43	0.0000E+00	0.0000E+00
X44	0.0000E+00	0.0000E+00
X45	0.0000E+00	0.0000E+00
ELEV	0.0000E+00	0.0000E+00
ELEVDD	0.0000E+00	0.0000E+00
ELEVDD	0.0000E+00	0.0000E+00
AIL	0.0000E+00	0.0000E+00
AILD	0.0000E+00	0.0000E+00
AILDD	0.0000E+00	0.0000E+00
WIND1	0.0000E+00	0.0000E+00
WIND2	0.0000E+00	0.0000E+00
ENOISE	0.0000E+00	0.0000E+00
ANOISE	0.0000E+00	0.0000E+00

	W <sub>1</sub>	W <sub>2</sub>	W <sub>3</sub>
X1	0.0000E+00	0.0000E+00	0.0000E+00
X2	0.0000E+00	0.0000E+00	0.0000E+00
X3	0.0000E+00	0.0000E+00	0.0000E+00
X4	0.0000E+00	0.0000E+00	0.0000E+00
X5	0.0000E+00	0.0000E+00	0.0000E+00
X6	0.0000E+00	0.0000E+00	0.0000E+00
X7	0.0000E+00	0.0000E+00	0.0000E+00
X8	0.0000E+00	0.0000E+00	0.0000E+00
X9	0.0000E+00	0.0000E+00	0.0000E+00
X10	0.0000E+00	0.0000E+00	0.0000E+00
X11	0.0000E+00	0.0000E+00	0.0000E+00
X12	0.0000E+00	0.0000E+00	0.0000E+00
X13	0.0000E+00	0.0000E+00	0.0000E+00
X14	0.0000E+00	0.0000E+00	0.0000E+00
X15	0.0000E+00	0.0000E+00	0.0000E+00
X16	0.0000E+00	0.0000E+00	0.0000E+00
X17	0.0000E+00	0.0000E+00	0.0000E+00
X18	0.0000E+00	0.0000E+00	0.0000E+00
X19	0.0000E+00	0.0000E+00	0.0000E+00
X20	0.0000E+00	0.0000E+00	0.0000E+00
X21	0.0000E+00	0.0000E+00	0.0000E+00
X22	0.0000E+00	0.0000E+00	0.0000E+00
X23	0.0000E+00	0.0000E+00	0.0000E+00
X24	0.0000E+00	0.0000E+00	0.0000E+00
X25	0.0000E+00	0.0000E+00	0.0000E+00
X26	0.0000E+00	0.0000E+00	0.0000E+00
X27	0.0000E+00	0.0000E+00	0.0000E+00
X28	0.0000E+00	0.0000E+00	0.0000E+00
X29	0.0000E+00	0.0000E+00	0.0000E+00
X30	0.0000E+00	0.0000E+00	0.0000E+00
X31	0.0000E+00	0.0000E+00	0.0000E+00
X32	0.0000E+00	0.0000E+00	0.0000E+00
X33	0.0000E+00	0.0000E+00	0.0000E+00
X34	0.0000E+00	0.0000E+00	0.0000E+00
X35	0.0000E+00	0.0000E+00	0.0000E+00
X36	0.0000E+00	0.0000E+00	0.0000E+00
X37	0.0000E+00	0.0000E+00	0.0000E+00
X38	0.0000E+00	0.0000E+00	0.0000E+00
X39	0.0000E+00	0.0000E+00	0.0000E+00
X40	0.0000E+00	0.0000E+00	0.0000E+00
X41	0.0000E+00	0.0000E+00	0.0000E+00
X42	0.0000E+00	0.0000E+00	0.0000E+00
X43	0.0000E+00	0.0000E+00	0.0000E+00
X44	0.0000E+00	0.0000E+00	0.0000E+00
X45	0.0000E+00	0.0000E+00	0.0000E+00
ELEV	0.0000E+00	0.0000E+00	0.0000E+00
ELEV0	0.0000E+00	0.0000E+00	0.0000E+00
ELEV00	0.0000E+00	8.0000E+05	0.0000E+00
AIL	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00
AILO0	0.0000E+00	0.0000E+00	8.0000E+05
WIND1	0.3713	0.0000E+00	0.0000E+00
WIND2	1.2450	0.0000E+00	0.0000E+00
ENOISE	0.0000E+00	1.0000	0.0000E+00
ANOISE	0.0000E+00	0.0000E+00	1.0000

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	X1	X2	X3	X4	X5	X6	X7	X8	X9	X10
QCG WTIPDD	4.4247E-05 35.92	4.3403E-05 -12.46	4.9713E-05 -0.5332	4.5556E-05 -0.5659	-4.1311E-06 -0.9664	7.9201E-06 12.75	7.2496E-06 -21.45	-6.7385E-05 6.822	-1.8236E-04 33.88	2.0657E-05 17.00
QCG WTIPDD	1.3194E-04 -0.1380	-1.5849E-04 -0.8803	-6.7655E-05 5.465	-8.7358E-06 -1.614	-9.8119E-05 55.18	3.1119E-05 30.10	-5.7479E-05 -4.878	3.1600E-04 14.36	-5.7750E-04 62.54	7.1000E-04 55.18
QCG WTIPDD	-9.6843E-05 -138.8	2.9934E-05 -104.4	5.4014E-04 6.831	-4.7620E-04 -11.78	-4.1630E-06 -55.04	-2.1609E-04 -30.66	-1.0541E-04 1.402	-3.1883E-05 -30.33	-1.5062E-04 4.869	-2.7714E-04 -74.28
QCG WTIPDD	-2.4361E-04 74.14	2.7990E-05 16.30	-1.6592E-04 3.118	1.2748E-05 8.728	-2.0762E-05 -74.53	-1.2546E-04 1.460	-4.4360E-05 -3.334	-1.0147E-05 -7.367	1.5343E-04 -1.032	2.1956E-05 2.867
QCG WTIPDD	-2.9386E-05 6.583	6.5513E-05 -1.361	6.1813E-05 1.350	1.9995E-05 18.71	8.9674E-06 -25.91	0.0000E+00 48.52	0.0000E+00 -7.932	0.0000E+00 7.9915E-02	0.0000E+00 -2.5618E+04	0.0000E+00 -167.4
QCG WTIPDD	0.0000E+00 0.2213	0.0000E+00 0.0000E+00	0.0000E+00 1.880	0.0000E+00 0.0000E+00	0.0000E+00 0.0000E+00					

	X1	X2	X3	X4	X5	X6	X7	X8	X9	X10
SHRI	-289.4	-189.2	54.94	64.24	131.2	53.66	159.9	70.45	-118.0	-29.86
BMOMI	-1.0116E+04	-9214.	1.3756E+04	2.1545E+04	1.3593E+04	1.7694E+04	-2984.	-3842.	-1.7279E+04	1314.
TORI	-3.5918E+04	-1.8298E+04	1444.	2675.	1.6733E+04	7353.	3.4725E+04	1.1489E+04	3528.	9170.
SHRO	-1.008	-5.628	22.26	24.73	5.535	17.55	4.685	-1.131	-17.83	-4.323
BMOMO	8616.	-576.7	1146.	1214.	-372.5	5513.	-3328.	1084.	8362.	5560.
TORO	-3685.	1359.	546.4	605.3	71.67	-1539.	2550.	-599.8	2050.	1803.
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

	X11	X12	X13	X14	X15	X16	X17	X18	X19	X20
SHRI	102.8	101.8	6.222	-19.80	-234.1	-168.5	33.07	17.06	237.5	253.3
BMOMI	3.2923E+04	3.3817E+04	-1082.	3076.	-3.3871E+04	-3.6494E+04	-7058.	1.1182E+04	8502.	1.0350E+04
TORI	3849.	3825.	-3369.	-1.0423E+04	-4762.	-1033.	-0.8833	4619.	3448.	1303.
SHRO	37.01	38.72	-4.403	-3.027	-27.42	-23.76	-13.45	2.659	-49.80	-48.30
BMOMO	1935.	2152.	839.2	-882.3	1.1555E+04	9556.	655.9	2046.	8408.	7455.
TORO	786.8	911.5	-899.7	-540.4	-1427.	-1640.	-693.1	3405.	1955.	530.8
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

	X21	X22	X23	X24	X25	X26	X27	X28	X29	X30
SHRI	7.799	97.62	-29.15	5.759	-33.32	-7.012	-103.5	-139.6	-159.0	-326.0
BMOMI	-5.7674E+04	-5.8520E+04	-9678.	-1.7572E+04	-4136.	-493.0	152.7	-2391.	-5.4007E+04	1.4065E+04
TORI	-1.6288E+04	917.4	-6520.	-4420.	1.3953E+04	1.0935E+04	-1.2971E+04	2265.	-6697.	-6.6463E+04
SHRO	-37.52	-36.55	3.951	-4.938	6.345	5.479	25.88	34.74	-62.23	-10.69
BMOMO	-6012.	-5724.	-3113.	-2967.	1289.	583.2	-6625.	-5544.	-2987.	2461.
TORO	-1239.	-1711.	-5337.	-5925.	7784.	6242.	-8377.	-2130.	-2052.	8424.
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

	X31	X32	X33	X34	X35	X36	X37	X38	X39	X40
SHRI	287.0	14.71	-11.49	93.88	203.2	-1.189	1.220	1.539	0.8601	1.222
BMOMI	-1.8204E+04	-4219.	-1617.	4.2055E+04	3.3610E+04	95.83	-530.3	-423.9	-30.47	560.5
TORI	5.9803E+04	-4749.	-3525.	-6148.	2.4850E+04	137.6	-1595.	-2912.	-203.6	2433.
SHRO	10.05	-16.66	-2.834	55.84	28.73	0.2784	-1.598	-2.559	-0.3003	1.781
BMOMO	-3217.	2832.	324.2	7562.	-1.2172E+04	9.422	-27.31	0.5400	-0.7739	14.79
TORO	-8033.	159.6	-1013.	-4374.	9713.	-41.64	-7.796	20.11	25.14	56.85
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00

	X41	X42	X43	X44	X45	ELEV	ELEV D	ELEVDD	AIL	AILD
SHRI	6.416	0.6052	-0.5647	-97.82	-1.384	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
BMOMI	667.4	-20.59	28.40	-3.2517E+04	-1345.	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
TORI	3134.	-170.6	202.4	-1.4519E+04	-691.2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
SHRO	2.065	-0.1941	0.2183	-35.76	-1.258	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
BMOMO	5.506	-2.632	2.610	1184.	-38.55	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
TORO	-202.9	1.613	1.493	-7454.	-471.2	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.000	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	1.000	0.0000E+00

	AILOD	WIND1	WIND2	ENOISE	ANOISE
SHRI	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
BMOMI	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
TORI	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
SHRO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
BMOMO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
TORO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
ELD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
EL	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILOD	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
AILO	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00



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	X1	X2	X3	X4	X5	X6	X7	X8	X9	X10
ELEV	1.5832E-04	-2.3582E-04	1.1357E-04	1.3312E-04	-4.1426E-05	4.2676E-05	2.6735E-04	1.7564E-04	-9.1525E-06	-1.9235E-05
AILC	3.0315E-03	2.6654E-03	4.1031E-04	7.3271E-04	1.4585E-04	-3.5377E-04	-1.2540E-03	4.6786E-04	1.3813E-06	-6.7161E-05
	X11	X12	X13	X14	X15	X16	X17	X18	X19	X20
ELEV	2.1995E-04	-4.5889E-05	-1.7194E-06	-4.3851E-05	-8.0336E-05	-2.5128E-05	-6.4003E-06	9.7488E-06	-2.4859E-06	1.1835E-05
AILC	9.5182E-04	3.5894E-04	6.2767E-05	3.7742E-04	-9.2428E-05	6.5354E-04	4.6382E-05	-2.8777E-04	-1.6007E-04	-1.7710E-04
	X21	X22	X23	X24	X25	X26	X27	X28	X29	X30
ELEV	-3.6349E-06	7.3601E-06	-1.4395E-05	-3.0966E-06	-2.9199E-05	7.3229E-06	2.0059E-05	1.9455E-06	-5.0617E-05	-1.4932E-05
AILC	2.4929E-04	8.8603E-05	3.1912E-04	2.5139E-04	-1.1683E-04	-9.9825E-04	2.7410E-04	7.8487E-04	-9.1330E-04	-6.2633E-04
	X31	X32	X33	X34	X35	X36	X37	X38	X39	X40
ELEV	2.9402E-05	6.3263E-06	2.3606E-06	-7.1657E-05	1.0550E-05	-2.3694E-08	6.8456E-08	1.2641E-08	3.0596E-10	4.0774E-07
AILC	5.0017E-04	-5.6772E-05	1.5107E-05	1.5403E-03	1.0277E-03	-9.3926E-08	-5.9855E-07	-3.5760E-07	3.5076E-07	5.9781E-06
	X41	X42	X43	X44	X45	ELEV	ELEV0	ELEVDD	AIL	AILD
ELEV	-2.3662E-07	9.0481E-10	-5.4855E-10	3.9594E-06	1.6946E-09	-0.4132	-6.8441E-03	-6.4513E-06	-2.1111E-02	-2.7671E-04
AILC	6.4990E-06	-2.7729E-09	5.3934E-09	-3.8792E-04	-3.7901E-08	-0.6329	-7.2630E-03	-7.0158E-06	-1.360	-2.1233E-02
	AILD0	WIND1	WIND2	ENOISE	ANOISE					
ELEV	-2.8063E-07	8.0010E-05	1.0842E-04	3.541	0.1928					
AILC	-2.0544E-05	2.2294E-04	1.4034E-03	2.677	8.327					

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	QCG	WTIPDD
X1	1785.	2.272
X2	3319.	2.6873E-02
X3	70.88	2.3472E-02
X4	554.4	2.5272E-02
X5	-689.6	-0.2266
X6	-43.74	0.1884
X7	-39.38	-9.2332E-02
X8	-108.3	4.5919E-02
X9	-105.6	0.2794
X10	777.9	0.2092
X11	1.8692E+04	4.8515E-02
X12	-9112.	-1.195
X13	2483.	-0.3082
X14	8.407	-2.693
X15	3332.	4.719
X16	6892.	0.1216
X17	189.0	0.1776
X18	-14.07	-0.3136
X19	-698.0	-0.6674
X20	960.5	-0.7365
X21	50.55	0.2265
X22	-6.130	9.7791E-02
X23	306.2	0.1553
X24	44.03	5.8746E-02
X25	-2799.	-5.225
X26	634.2	0.6398
X27	1756.	-1.150
X28	3578.	-0.9081
X29	3122.	0.3963
X30	13.31	-2.7236E-02
X31	-30.99	0.1238
X32	6683.	1.259
X33	-8069.	-0.6234
X34	-7828.	0.6847
X35	8314.	4.343
X36	86.05	1.0999E-02
X37	-20.95	9.2423E-02
X38	43.47	-9.7774E-02
X39	82.23	5.1789E-02
X40	-296.3	-0.2155
X41	60.50	1.2172E-02
X42	-20.62	-9.3657E-03
X43	18.70	4.0876E-04
X44	7830.	3.815
X45	2354.	1.587
ELEV	0.8878	-4.1163E-06
ELEV0	11.43	-1.2973E-03
ELEVDD	380.9	1.298
AIL	-3.558	1.2771E-03
AILD	-98.84	-0.5599
AILD0	1.7817E+04	40.63
WIND1	-4600.	-2.597
WIND2	-1.3619E+04	-8.357
ENOISE	-1.9461E-02	3.3987E-08
ANOISE	-0.3878	-3.7938E-04