

Cooperative Localisation of a GPS-Denied UAV in 3-Dimensional Space Using Direction of Arrival Measurements ^{*}

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Abstract: This paper presents a novel approach for localising a GPS (Global Positioning System)-denied Unmanned Aerial Vehicle (UAV) with the aid of a GPS-equipped UAV in three-dimensional space. The GPS-equipped UAV makes discrete-time broadcasts of its global coordinates. The GPS-denied UAV receives the broadcast and in doing so takes a direction of arrival (DOA) measurement towards the origin of the broadcast in its local coordinate frame (obtained via an inertial navigation system (INS)). The aim is to determine the difference between the local and global frames, described by a rotation and a translation. In the noiseless case, global coordinates are recovered exactly by solving a system of linear equations. When DOA measurements are contaminated with noise, rank relaxed semidefinite programming (SDP) and the Orthogonal Procrustes algorithm are employed. Simulations are provided and factors affecting accuracy, such as noise levels and number of measurements, are explored.

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1. INTRODUCTION

Unmanned aerial vehicles play a central role in many defence reconnaissance and surveillance operations. Formations of UAVs can provide greater reliability and coverage when compared to a single UAV. To provide meaningful data in such operations, all UAVs in a formation must have a common reference frame (typically the global frame). Traditionally, UAVs have access to the global frame via GPS. However, GPS signals may be lost in urban environments and enemy controlled airspace (jamming).

Without access to global coordinates, a UAV must rely on its inertial navigation system (INS). Positions in the INS frame are updated by integrating measurements from gyroscopes and accelerometers. Error in these measurements causes the INS frame to accumulate drift. At any given time, drift can be characterised by rotation and translation with respect to the global frame, and is assumed to be independent between UAVs in a formation. The error in gyroscope and accelerometer readings is stochastic. As a result, INS frame drift cannot be modelled deterministically. Information from both the global and INS frames must be collected and used to determine the drift between

frames. This process is described as cooperative localisation when multiple vehicles provide information.

Various measurement types such as distance between agents and direction of arrival of a signal (we henceforth call DOA) can be used for this process. In the context of UAVs, additional sensors add weight and consume power. As a result, one generally aims to minimise the number of measurement types required for localisation. This paper studies a cooperative approach to localisation using DOA measurements.

We begin a review of existing literature involving DOA measurements by distinguishing localisation from tracking. A tracking problem typically involves updating a solution in real time, as new measurements are made available. Tracking is performed using Bayesian filters such as particle filters (Lin and Wei, 2013) and the Extended Kalman Filter (Chang and Fang, 2014) (Chunshi et al., 2011). In localisation, a set of measurements collected over a time interval is used to compute a solution at the end of the interval. A dynamic model is typically not required in localisation, and is not used in this paper. In (Tekdas and Isler, 2010), a target is localised using

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bearing¹ measurements taken in the global frame by a stationary sensor network. In (Duan et al., 2012), self-localisation of a robot is achieved by taking bearing-only measurements from the robot's INS frame towards a set of landmarks with known global positions. (Bayram et al., 2016) demonstrates how an agent is able to localise a stationary target using bearing-only measurements. Optimal path planning algorithms allowing GPS-enabled sensing agents to localise a fixed target are studied in (Lim and Bang, 2014). (Ye et al., 2017) completed formation control tasks for multiple agents by using a method of self-localisation using bearing-measurements. Simultaneous localisation and mapping (SLAM) methods allow for self-localisation using only INS positions and bearing measurements (Mohammadloo et al., 2013). (Bailey, 2003). The local frame is anchored by positions of landmarks which are generally stationary in the global frame and known a priori or continuously sensed.

The problem addressed in this paper is to localise a GPS-denied UAV, which we will call Agent B, with the assistance of a nearby GPS-enabled UAV, which we will call Agent A. Agent A broadcasts its global coordinates at discrete instants in time. Both agents move about arbitrarily in three-dimensional space. For each broadcast of Agent A, Agent B is able to take a DOA measurement towards Agent A.

This problem and the solution proposed in this paper are novel. In particular, while the literature discussed above considers certain aspects from the following list, none consider all of the following aspects simultaneously:

- The network consists of only two mobile agents (and is therefore different to the sensor network localisation problems in the literature).
- There is no a priori knowledge or sensing of a stationary reference point in the global frame.
- The UAVs execute unconstrained arbitrary motion in three-dimensional space.
- Cooperation between a GPS-enabled and a GPS-denied UAV (transmission of signals is unidirectional; from Agent A to Agent B).

(Zhang et al., 2016) studied this problem in two-dimensional space using bearing measurements. One single piece of data is acquired at each time step. As will be made clear in the sequel, two scalar quantities are obtained with each DOA measurement in the three-dimensional case, requiring new techniques to be introduced.

The rest of the paper is structured as follows. In Section 2 the problem is formalised. In Section 3, a solution to the noiseless case is presented. Section 4 extends this method to allow for noise in DOA measurements. Section 5 presents simulation results for the noisy measurement case. The paper is concluded in Section 6.

2. PROBLEM DEFINITION

Two agents, which we call Agent A and Agent B, follow arbitrary trajectories in three-dimensional space. Agent A

has GPS and therefore navigates with respect to the global frame (which we will also refer to as the coordinate frame of Agent A). Because Agent B is GPS-denied, it has no self-localisation capacity in the global frame, but can self-localise and navigate in an INS frame. This INS frame drifts with respect to the global frame over long periods, but can be considered constant in short intervals.

Positions of each agent in their respective navigation frames and DOA measurements of signals between agents are obtained through a discrete-time measurement process. We let $P_J^I(k)$ denote the position of agent J in the coordinate frame of agent I at the k^{th} time instant. Time between measurements can be variable. Let u, v, w denote global frame coordinates, and x, y, z denote coordinates in the INS frame of Agent B. Position coordinates at time instant k are expressed as follows:

$$P_A^A(k) = [u_A(k) \ v_A(k) \ w_A(k)]^\top \quad (1)$$

$$P_B^B(k) = [x_B(k) \ y_B(k) \ z_B(k)]^\top \quad (2)$$

Agent B's INS frame evolves via drift which, at a particular time instant, can be modelled as a rotation and a translation from the global frame. The rotation and origin of the INS frame is considered to be time invariant over short intervals, during which the following measurement process occurs multiple times. At each time instant k :

- Agent A records and broadcasts its position in the global frame, i.e. $P_A^A(k)$.
- Agent B records its own position in the INS frame, i.e. $P_B^B(k)$.
- Agent B receives the broadcast $P_A^A(k)$ from Agent A, and measures the signal's DOA. Measurement may be made with a Radio Frequency (RF) antenna or an optical camera.

We assume the delay between Agent A sending its coordinates and Agent B receiving this information is negligible, i.e. we assume the three activities occur simultaneously.

The aim is to determine the coordinates of Agent B in the global frame:

$$P_B^A(k) = [u_B(k) \ v_B(k) \ w_B(k)]^\top \quad (3)$$

Passing between the global frame and the INS frame of Agent B is achieved by a rotation of frame axes and translation of origin point of the frame. For instance, the coordinates of Agent A in the INS frame of Agent B is:

$$P_A^B = \mathbf{R}_A^B P_A^A + \mathbf{T}_A^B \quad (4)$$

We therefore have $P_A^B = \mathbf{R}_A^B P_A^A + \mathbf{T}_A^B$ where $\mathbf{R}_A^B = \mathbf{R}_A^B$ and $-\mathbf{R}_A^B \mathbf{T}_A^B = \mathbf{T}_A^B$. The localisation problem can therefore be reduced to solving for $\mathbf{R}_A^B \in SO(3)$ with entries r_{ij} and $\mathbf{T}_A^B \in \mathbb{R}^3$ with entries t_i . DOA measurements taken by Agent B towards Agent A are performed by instruments fixed to the body of Agent B, whose rotation within the INS frame is known.

A DOA measurement, referenced to the INS frame, is expressed using the following spherical coordinate system:

- Azimuth (θ): angle formed between the positive x axis and the projection of the vector from Agent B towards Agent A onto the xy plane.
- Elevation (ϕ): angle formed between the unit vector towards Agent A and xy plane. The angle is positive

¹ The term bearing is used interchangeably with direction of arrival (DOA) in a two-dimensional ambient space. However, we refrain from using it in three-dimensional ambient space

if the z component of the unit vector towards Agent A is positive.

The total number of scalar measurements required to solve the localisation problem cannot be smaller than the number of degrees of freedom in the rotation matrix and translation vector. Note that $\mathbf{R}_A^B \in SO(3)$ has different possible parametrisations. Euler angle parametrisation of \mathbf{R}_A^B is a 3-vector of Euler angles. The translation vector is a 3-vector. This problem therefore has 6 degrees of freedom. In this paper, we work directly with entries r_{ij} ; as will be made clear in the sequel, this allows us to solve linear equations.

The matrix \mathbf{R}_A^B is a rotation matrix if and only if $\mathbf{R}_A^B \mathbf{R}_A^{B\top} = I_3$ and $\det(\mathbf{R}_A^B) = 1$. As will be seen in the sequel, these constraints are equivalent to a set of quadratic constraints on the entries of \mathbf{R}_A^B . In total there are 12 entries of \mathbf{R}_A^B and \mathbf{T}_A^B to be found as we work directly with r_{ij} . An equation set of n independent relations (including measurements and constraints) for n variables will generically have multiple solutions if at least one of the relations is quadratic. When an additional scalar measurement is taken, generically a unique solution exists.

3. LOCALISATION WITH NOISELESS MEASUREMENTS

This section considers noiseless position and direction of arrival measurements. Section 4 considers noise in direction of arrival measurements only. The consideration of noisy position measurements is left for future work.

3.1 Forming a system of linear equations

A unit vector in the INS frame, pointing from Agent B to Agent A, defined by azimuth and elevation angles θ and ϕ , is given by:

$$\hat{d}(\theta, \phi) = [\cos \theta \cos \phi, \sin \theta \cos \phi, \sin \phi]^\top \quad (5)$$

The following analysis holds for all k instants in time, hence we drop the argument k . Define $\bar{d} \doteq \|P_B^A - P_B^B\|$ as the Euclidean distance between Agent A and Agent B (which is not available to either agent). Scaling the unit vector \hat{d} gives

$$\bar{d}(\theta, \phi) = \frac{1}{\bar{d}} [x_A - x_B, y_A - y_B, z_A - z_B]^\top \quad (6)$$

Applying equation (4) yields:

$$\begin{bmatrix} \cos \theta \cos \phi \\ \sin \theta \cos \phi \\ \sin \phi \end{bmatrix} = \frac{1}{\bar{d}} \begin{bmatrix} r_{11}u_A + r_{12}v_A + r_{13}w_A + t_1 - x_B \\ r_{21}u_A + r_{22}v_A + r_{23}w_A + t_2 - y_B \\ r_{31}u_A + r_{32}v_A + r_{33}w_A + t_3 - z_B \end{bmatrix} \quad (7)$$

The left hand vector is calculated directly from DOA measurements. Cross-multiplying entries 1 and 3 of both vectors eliminates \bar{d} , and yields:

$$\begin{aligned} \sin \phi (r_{11}u_A + r_{12}v_A + r_{13}w_A + t_1 - x_B) = \\ \cos \theta \cos \phi (r_{31}u_A + r_{32}v_A + r_{33}w_A + t_3 - z_B) \end{aligned} \quad (8)$$

which for convenience is rearranged as

$$\begin{aligned} (u_A \sin \phi) r_{11} + (v_A \sin \phi) r_{12} + (w_A \sin \phi) r_{13} \\ - (u_A \cos \theta \cos \phi) r_{31} - (v_A \cos \theta \cos \phi) r_{32} \\ - (w_A \cos \theta \cos \phi) r_{33} + (\sin \phi) t_1 - (\cos \theta \cos \phi) t_3 \\ = (\sin \phi) x_B - (\cos \theta \cos \phi) z_B \end{aligned} \quad (9)$$

Similarly, cross-multiplying entries 2 and 3 of both vectors appearing in (7) yields a similar equation.

$$\begin{aligned} (u_A \sin \phi) r_{21} + (v_A \sin \phi) r_{22} + (w_A \sin \phi) r_{23} \\ - (u_A \sin \theta \cos \phi) r_{31} - (v_A \sin \theta \cos \phi) r_{32} \\ - (w_A \sin \theta \cos \phi) r_{33} + (\sin \phi) t_2 - (\sin \theta \cos \phi) t_3 \\ = (\sin \phi) y_B - (\sin \theta \cos \phi) z_B \end{aligned} \quad (10)$$

Notice that both equations (9) and (10) are linear in the unknown r_{ij} and t_i terms. Given a series of K DOA measurements (each giving $\phi(k), \theta(k)$), (9) and (10) can be used to construct the following system of linear equations:

$$A\Psi = b, \quad A \in \mathbb{R}^{2K \times 12} \quad (11)$$

where the 12-vector of unknowns Ψ is defined as:

$$\Psi = [r_{11} \ r_{12} \ r_{13} \ \dots \ r_{31} \ r_{32} \ r_{33} \ t_1 \ t_2 \ t_3]^\top \quad (12)$$

The matrix A contains products and functions of the known values $P_A^A(k)$ and $\phi(k), \theta(k)$ for $k = 1, \dots, K$. The vector b contains the known values $P_B^B(k)$ and $\phi(k), \theta(k)$ for $k = 1, \dots, K$. The precise forms of A and b are omitted due to space limitations.

3.2 Example with noiseless DOA measurements

If $K \geq 6$, the matrix A will be square or tall. In the noiseless case, if A is of full column rank, equation (11) will be solvable. An example trajectory was created for Agent A and for Agent B over 6 time instants. These trajectories are plotted in Figure 1. Rotation and translation of Agent B's INS frame was generated randomly. Entries of \mathbf{R}_A^B and \mathbf{T}_A^B were recovered exactly. Due to space limitations, we omit all position data, INS frame rotation and translation data from this paper. This data is available in an extended version of this paper found on ArXiv (Russell et al., 2017).

3.3 Nongeneric trajectories

It is obvious that we can only localise Agent B by solving (11) if matrix A has full column rank. We are therefore motivated to identify trajectories of Agent A and Agent B which result in $\text{rank}(A) < 6$ (assuming $K \geq 6$) so we can avoid them. A large number of simulations revealed that $\text{rank}(A) < 6$ is consistently encountered for all $K \geq 6$ when the trajectory of Agent A is restricted to a plane. Note that this plane need not be parallel to a coordinate plane of either the global or INS coordinate frames. We leave further, detailed analytical treatment of nongeneric trajectories as future work.

4. LOCALISATION WITH NOISY DOA MEASUREMENTS

This section develops an approach to deal with noisy DOA measurements from sensors on Agent B, which will be encountered in real-world implementation. We approach the problem using semidefinite programming to exploit the quadratic constraints on certain entries of Ψ arising from the properties of the rotation matrix. Such constraints are not used in an unconstrained least squares approach.

In practice, noise contaminated azimuth and elevation measurements are taken in the body fixed frame of Agent B. Strictly speaking, the noise is expected to follow a von Mises distribution (Forbes et al., 2011). For small noise,

such as what we encounter, the von Mises distribution can be approximated by a Gaussian distribution. The noise affecting azimuth and elevation are assumed to be independent when measured in the body fixed frame, however they are not known to have equal standard deviations. These noises are likely to lose independence when azimuth and elevation measurements measured in the body fixed frame are converted into azimuth and elevation values in Agent B's body centred frame, which has the same orientation as its INS frame.

4.1 Quadratic constraints on entries of Ψ

We now identify 21 quadratic constraints on entries of \mathbf{R}_A^B . Note that this set is not independent, as discussed in Remark 1 below. Recall the orthogonality property $\mathbf{R}_A^B \mathbf{R}_A^{B\top} = I_3$. By computing each entry of $\mathbf{R}_A^B \mathbf{R}_A^{B\top}$ and setting these equal to entries of I_3 , we define constraints C_i for $i = 1, \dots, 6$:

$$C_1 = \psi_1^2 + \psi_2^2 + \psi_3^2 - 1 = 0 \quad (13a)$$

$$C_2 = \psi_4^2 + \psi_5^2 + \psi_6^2 - 1 = 0 \quad (13b)$$

$$C_3 = \psi_7^2 + \psi_8^2 + \psi_9^2 - 1 = 0 \quad (13c)$$

$$C_4 = \psi_1\psi_4 + \psi_2\psi_5 + \psi_3\psi_6 = 0 \quad (13d)$$

$$C_5 = \psi_1\psi_7 + \psi_2\psi_8 + \psi_3\psi_9 = 0 \quad (13e)$$

$$C_6 = \psi_4\psi_7 + \psi_5\psi_8 + \psi_6\psi_9 = 0 \quad (13f)$$

To simplify notation we call $C_{j:k}$ the set of constraints C_i for $i = j, \dots, k$. Similarly, by computing each entry of $\mathbf{R}_A^{B\top} \mathbf{R}_A^B$ and setting these equal to I_3 , we define constraints $C_{7:12}$. We omit presentation of $C_{7:12}$ due to space limitations and similarity with $C_{1:6}$. The sets $C_{1:6}$ and $C_{7:12}$ are clearly equivalent.

Further constraints are required to ensure $\det(\mathbf{R}_A^B) = 1$. Cramer's formula states that $\mathbf{R}_A^{B-1} = \text{adj}(\mathbf{R}_A^B) / \det(\mathbf{R}_A^B)$, where $\text{adj}(\mathbf{R}_A^B)$ denotes the adjugate matrix of \mathbf{R}_A^B . Orthogonality of \mathbf{R}_A^B implies $\mathbf{R}_A^{B\top} = \text{adj}(\mathbf{R}_A^B)$ or that $\mathbf{R}_A^B = \text{adj}(\mathbf{R}_A^B)^\top$. By computing entries of the first column of $Z = \mathbf{R}_A^B - \text{adj}(\mathbf{R}_A^B)^\top$ and setting these equal to 0, we define constraints $C_{13:15}$:

$$C_{13} = \psi_1 - (\psi_5\psi_9 - \psi_6\psi_8) = 0 \quad (14a)$$

$$C_{14} = \psi_4 - (\psi_3\psi_8 - \psi_2\psi_9) = 0 \quad (14b)$$

$$C_{15} = \psi_7 - (\psi_2\psi_6 - \psi_3\psi_5) = 0 \quad (14c)$$

Similarly, by computing the entries of the second and third columns of Z and setting these equal to 0, we define constraints $C_{16:18}$ and $C_{19:21}$. Due to space limitations, we omit presenting them. The complete set $C_{1:21} \doteq C_\Psi$ constrains \mathbf{R}_A^B to be a rotation matrix.

Due to these additional relations, localisation requires azimuth and elevation measurements at 4 instants only ($K = 4$), as opposed to 6 instants required in Section 3.

4.2 Formulation of the Semidefinite Program

The goal of the semidefinite program is to obtain:

$$\underset{\Psi}{\text{argmin}} \|A\Psi - b\| \quad (15)$$

subject to C_Ψ . Equivalently, we seek $\underset{\Psi}{\text{argmin}} \|A\Psi - b\|^2$ subject to C_Ψ . We define the inner product of two matrices U and V as $\langle U, V \rangle = \text{trace}(UV^\top)$. One obtains

$$\|A\Psi - b\|^2 = \langle P, X \rangle \quad (16)$$

where $P = [A \ b]^\top [A \ b]$ and

$$X = \begin{bmatrix} \Psi \\ -1 \end{bmatrix} \begin{bmatrix} \Psi \\ -1 \end{bmatrix}^\top \quad (17)$$

and X is a rank 1 positive-semidefinite matrix². The constraints C_Ψ can also be expressed in inner product form. For $i = 1, \dots, 21$, $C_i = 0$ is equivalent to $\langle Q_i, X \rangle = 0$ for some Q_i . Solving for Ψ in (15) is therefore equivalent to solving for:

$$\underset{\Psi}{\text{argmin}} \langle P, X \rangle \quad (18)$$

such that:

$$X \geq 0 \quad (19)$$

$$\text{rank}(X) = 1 \quad (20)$$

$$X_{13,13} = 1 \quad (21)$$

$$\langle Q_i, X \rangle = 0 \quad (22)$$

for $i = 1, \dots, 21$. This fully defines the semidefinite program.

Remark 1. (Inclusion of Dependent Constraints). While the set of equations (13) and (14) form an independent set of constraints on the first nine entries of Ψ , the set of constraints C_Ψ is not independent. For instance, $C_{1:6}$ and $C_{7:12}$ are equivalent. For simplicity, we use C_Ψ in the SDP formulation in this paper.

Remark 2. (Normalisation of translation terms). It was observed that SDP solution accuracy deteriorates when the condition number of X of the true solution is high. When approximate size of \mathbf{T}_A^B is known, coefficients associated to entries t_i in equations (9) and (10) are scaled to solve for values close to 1.

4.3 Rank Relaxation of Semidefinite Program

This semidefinite program is a reformulation of a quadratically constrained quadratic program (QCQP). Computationally speaking, QCQP problems are generally NP-hard. A close approximation to the true solution can be obtained in polynomial time if the rank 1 constraint on X is relaxed. The solution to the relaxed semidefinite program X is typically close to being a rank 1 matrix³. The closest rank 1 approximation to X , which we call \hat{X} , is obtained by evaluating the singular value decomposition of X , then setting all singular values except the largest equal to zero.

From \hat{X} , one can then use the definition of X in (17) to obtain the approximation of Ψ , which we will call $\hat{\Psi}$. Entries $\hat{\psi}_i$ for $i = 10, 11, 12$ can be used immediately to construct an estimate for \mathbf{T}_A^B , which we will call \hat{T} . Entries $\hat{\psi}_i$ for $i = 1, \dots, 9$ will be used to construct an approximation of \mathbf{R}_A^B , which we will call \hat{R} .

4.4 Orthogonal Procrustes Problem

Due to the relaxation of the rank constraint on X , it is no longer guaranteed that entries of $\hat{\Psi}$ strictly satisfy the set of constraints C_Ψ . Specifically, the matrix \hat{R} may not be a rotation matrix. The Orthogonal Procrustes algorithm is

² All matrices M which can be expressed in the form of $M = vv'$ where v is a column vector are positive-semidefinite matrices.

³ The measure used for closeness to rank 1 is the ratio of the two largest singular values in the singular value decomposition of X .

a commonly used tool to determine the closest orthogonal matrix (denoted \bar{R}) to a given matrix, \hat{R} . This is given by $\bar{R} = \operatorname{argmin}_{\Omega} \|\Omega - \hat{R}\|_F$ subject to $\Omega\Omega^T = I$, where $\|\cdot\|_F$ is the Frobenius norm.

When noise is high, the above method occasionally returns \bar{R} such that $\det(\bar{R}) = -1$. A special case of the Orthogonal Procrustes algorithm is available to ensure that $\det(\bar{R}) = 1$, i.e. $\bar{R} \in SO(3)$ is a proper rotation matrix. We omit the minor details due to space limitations.

The matrix \bar{R} and vector \bar{T} are the final estimates of \mathbf{R}_A^B and \mathbf{T}_A^B from the semidefinite program and Orthogonal Procrustes methods. The estimate of Agent B's position in the global frame is $\bar{P}_B^A = \bar{R}^T (P_B^B - \bar{T})$.

4.5 Metrics for error in \bar{R} and \bar{T}

This paper uses the geodesic metric for rotation. This metric on $SO(3)$ defined by

$$d(R_1, R_2) = \arccos\left(\frac{\operatorname{tr}(R_1^T R_2) - 1}{2}\right) \quad (23)$$

is the magnitude of angle of rotation about this axis (Tron et al., 2016). Where \mathbf{R}_A^B is known, the error of rotation \bar{R} is defined as $d(\bar{R}, \mathbf{R}_A^B)$. Position error is defined as the average Euclidian distance between true global coordinates of B, and estimated global coordinates over the K measurements taken.

$$\operatorname{error}(\bar{P}_B^A) = \frac{\sum_k \|\bar{P}_B^A(k) - P_B^A(k)\|}{K} \quad (24)$$

5. SIMULATION RESULTS

In this section, we investigate the performance of the SDP algorithm combined with the Orthogonal Procrustes algorithm in the presence of noise (we shall call this combined algorithm SDP+O for short). We acknowledged in Section 4 that noise in measurements of $\theta(k)$ and $\phi(k)$ may not have the same standard deviations. However, for simplicity and with space limitations in mind, we will assume in this paper that the standard deviations are the same (which we denote as σ). In other words, $\tilde{\theta}(k) = \theta(k) + \zeta_1$ and $\tilde{\phi}(k) = \phi(k) + \zeta_2$ where $\zeta_1, \zeta_2 \sim N(\mu, \sigma^2)$. Extensive exploration of different standard deviations for $\theta(k)$ and $\phi(k)$ will be conducted as future work.

5.1 Example with noisy DOA measurements

Samples of Gaussian error with $\mu = 0^\circ$, $\sigma = 3^\circ$ were added to elevation and azimuth measurements in the example scenario simulated in Section 3.2. The SDP+O algorithm was used to obtain \bar{R} and \bar{T} . The reconstructed trajectory \bar{P}_B^A is plotted in Figure 1, and we can see Agent B has localised itself in the global frame with only a small error.

5.2 Monte Carlo Simulations on Random Trajectories

In this subsection, we conduct Monte Carlo simulations to show the viability of the SDP+O algorithm. We vary the noise level by $\sigma = 0.1^\circ, 1^\circ, 2^\circ, 3^\circ, 5^\circ$. The noise level $\sigma = 0.1^\circ$ is representative of an optical sensor, while

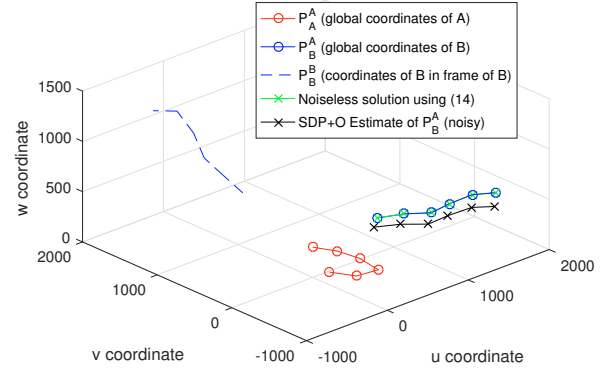


Fig. 1. Recovery of global coordinates of Agent B for example trajectories (error of $\sigma = 3$ in noisy case)

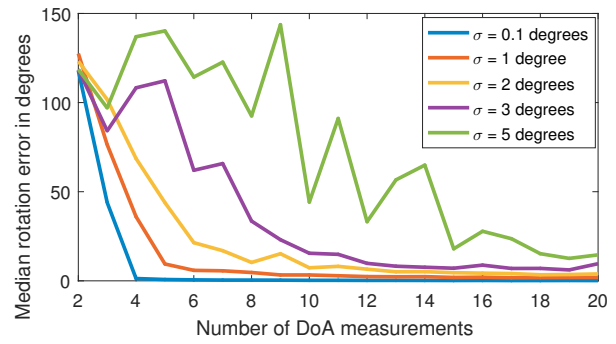


Fig. 2. Median $d(\bar{R}, \mathbf{R}_A^B)$ vs. number of DOA measurements used to solve SDP+O.

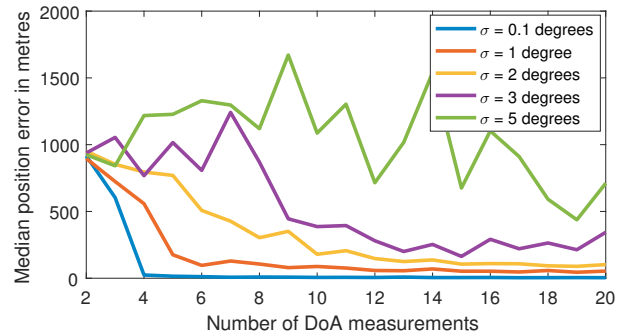


Fig. 3. Median $\operatorname{error}(\bar{P}_B^A)$ vs. number of DOA measurements used to solve SDP+O (average distance of 1.38km between agents).

other noise levels are representative of antenna-based (RF) measurements. For each level of noise, for each number of measurements K from 2 to 20, we simulated 100 unique and realistic UAV trajectories. By realistic, we mean that the distance separation between successive measurements is consistent with UAV flight speeds and ensures the UAV does not exceed an upper bound on the turn/climb rate. We calculated the median $d(\bar{R}, \mathbf{R}_A^B)$ and $\operatorname{error}(\bar{P}_B^A)$ over the 100 simulations, and plotted these in Figures 2 and 3.

To analyse the results, we look at the median, which is commonly used as a measure of central tendency to mitigate the effect of outliers. The median $d(\bar{R}, \mathbf{R}_A^B)$ and

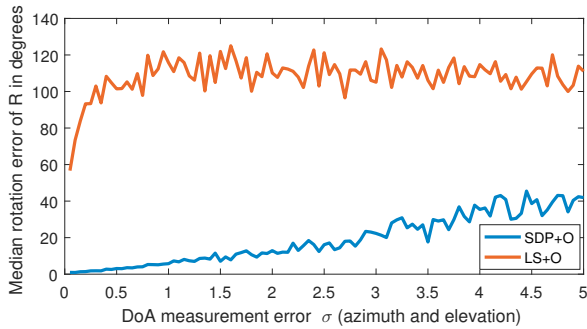


Fig. 4. Comparison of median $d(\bar{R}, \mathbf{R}_A^B)$ using SDP+O and LS+O methods for example trajectory ($K = 6$).

error (\bar{P}_B^A) versus the number of measurements (i.e. K) used to solve the SDP+O are plotted in Figure 2 and Figure 3, respectively. It is observed that for each value of σ there is greater improvement in rotation error than translation error as K is increased.

5.3 Comparison of LS+O and SDP+O

In this subsection, we compare the SDP+O algorithm with an unconstrained Least Squares algorithm combined with the Orthogonal Procrustes algorithm (which we call LS+O). By LS+O, we mean that $\Psi^* = \operatorname{argmin}_{\Psi} \|A\Psi - b\|$ is found without any constraints on Ψ . The first nine entries of Ψ are then used to form a matrix, and the Orthogonal Procrustes algorithm detailed in subsection 4.4 is applied to obtain the closest rotation matrix \bar{R} .

Agents A and B are prescribed the representative trajectories illustrated in Figure 1. Noise level was varied from $\sigma = 0^\circ$ to 5° . For each noise level, we conducted 20 Monte Carlo simulations of the same trajectory using LS+O and SDP+O. The error index $d(\bar{R}, \mathbf{R}_A^B)$ was separately calculated over the 20 simulations for LS+O and SDP+O. Figure 4 shows the median $d(\bar{R}, \mathbf{R}_A^B)$ versus level of noise for both LS+O and SDP+O. The median $d(\bar{R}, \mathbf{R}_A^B)$ using the LS+O algorithm was consistently more than double that using the SDP+O method. We conclude that SDP+O is the superior method. Its median performance is approximately linear in the mean azimuth and elevation measurement error standard deviation.

6. CONCLUSION

This paper studied a cooperative localisation problem between a GPS-denied and a GPS-enabled UAV. A localisation algorithm was developed in two stages. With noiseless DOA measurements, we showed that a linear system of equations built from six or more measurements yielded the localisation solution for generic trajectories. The second stage considered noisy DOA measurements, which we addressed numerically using a rank relaxed semidefinite program with the solution adjusted using the Orthogonal Procrustes algorithm. Simulations were presented to illustrate the effectiveness of the algorithm when DOA measurements were noisy. Future work includes improving the reliability of the SDP+O method. In addition, we aim to study multiple agents in a formation, and filtering methods.

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